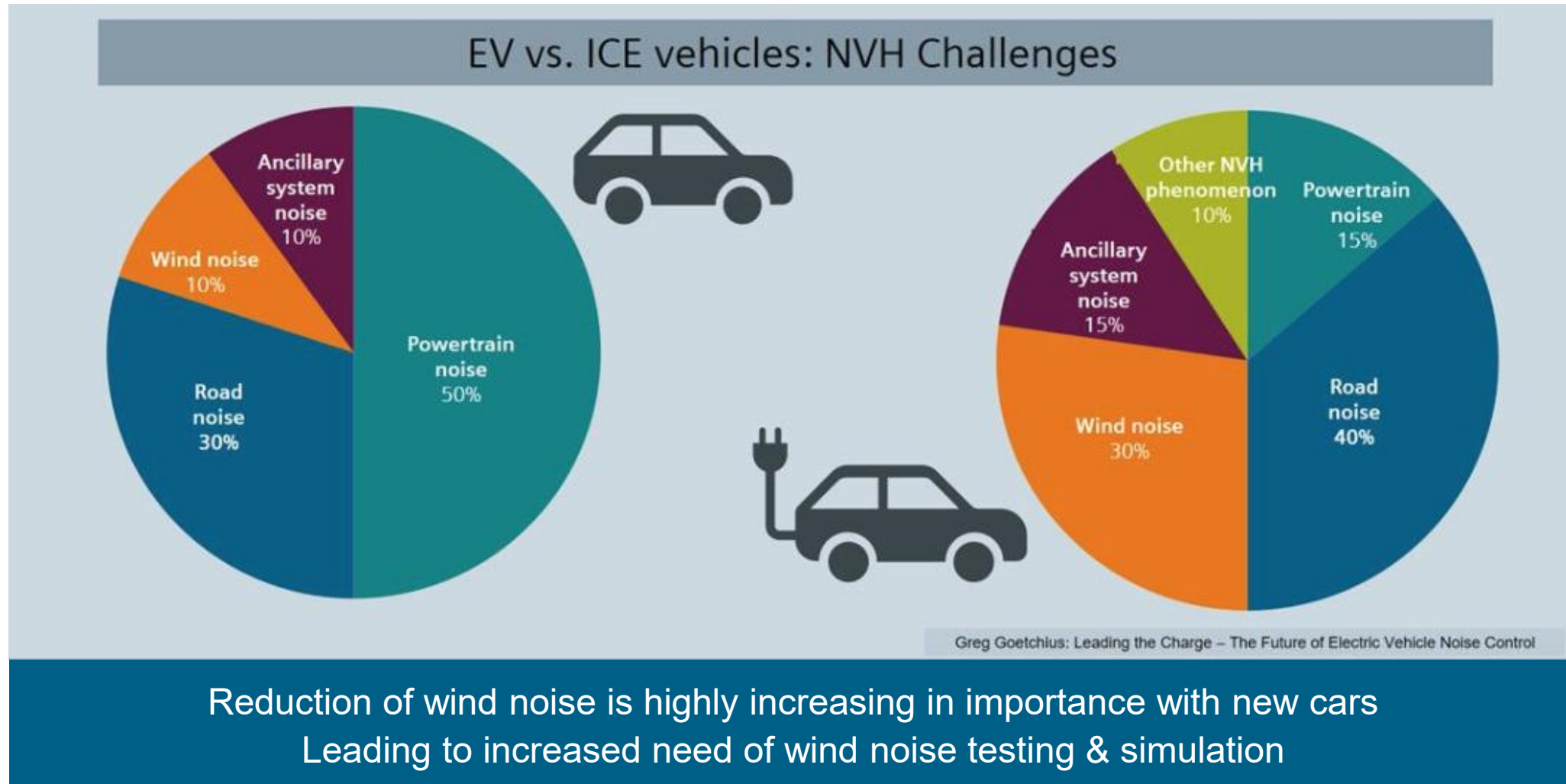


3 validated aero-(vibro)-acoustic scenarios to predict noise levels

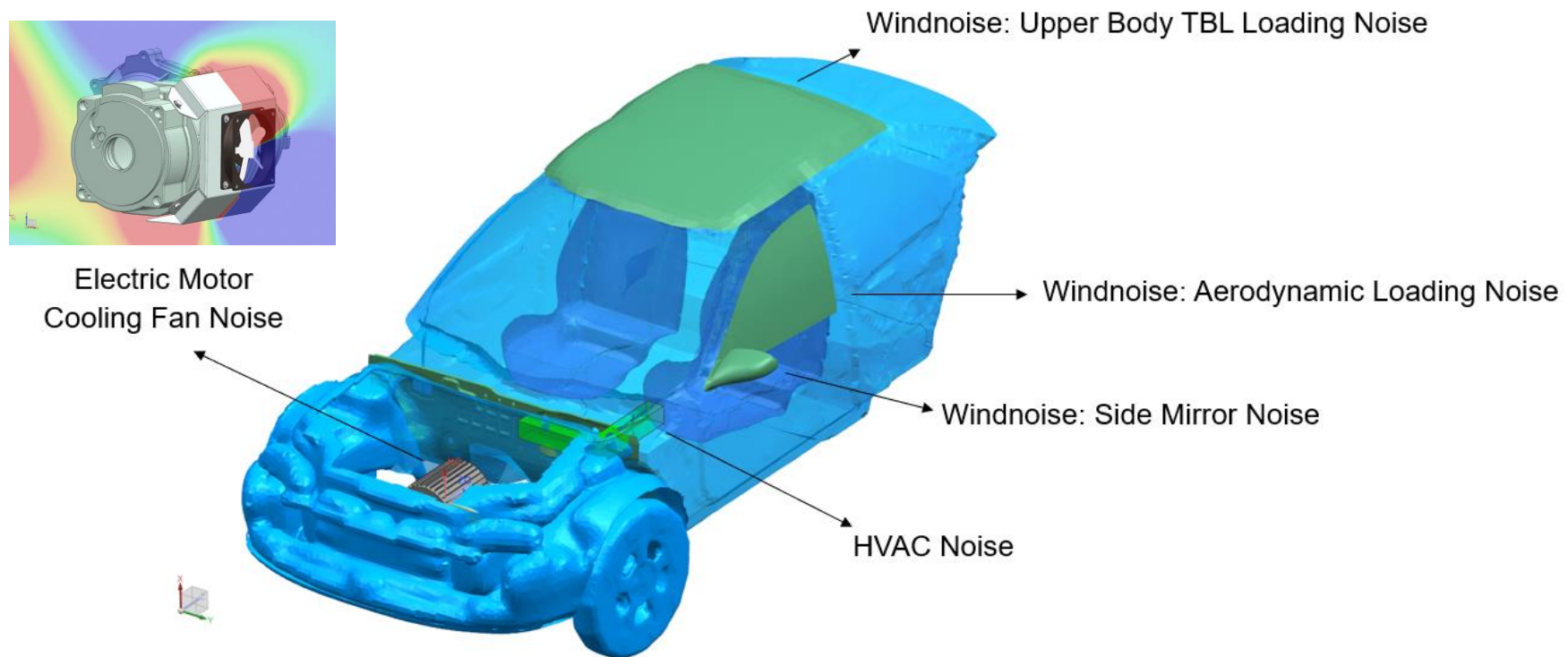
The supremacy of lean FE models to solve flow-induced wind, fan and HVAC noise

Shift towards increased effort to reduce wind noise



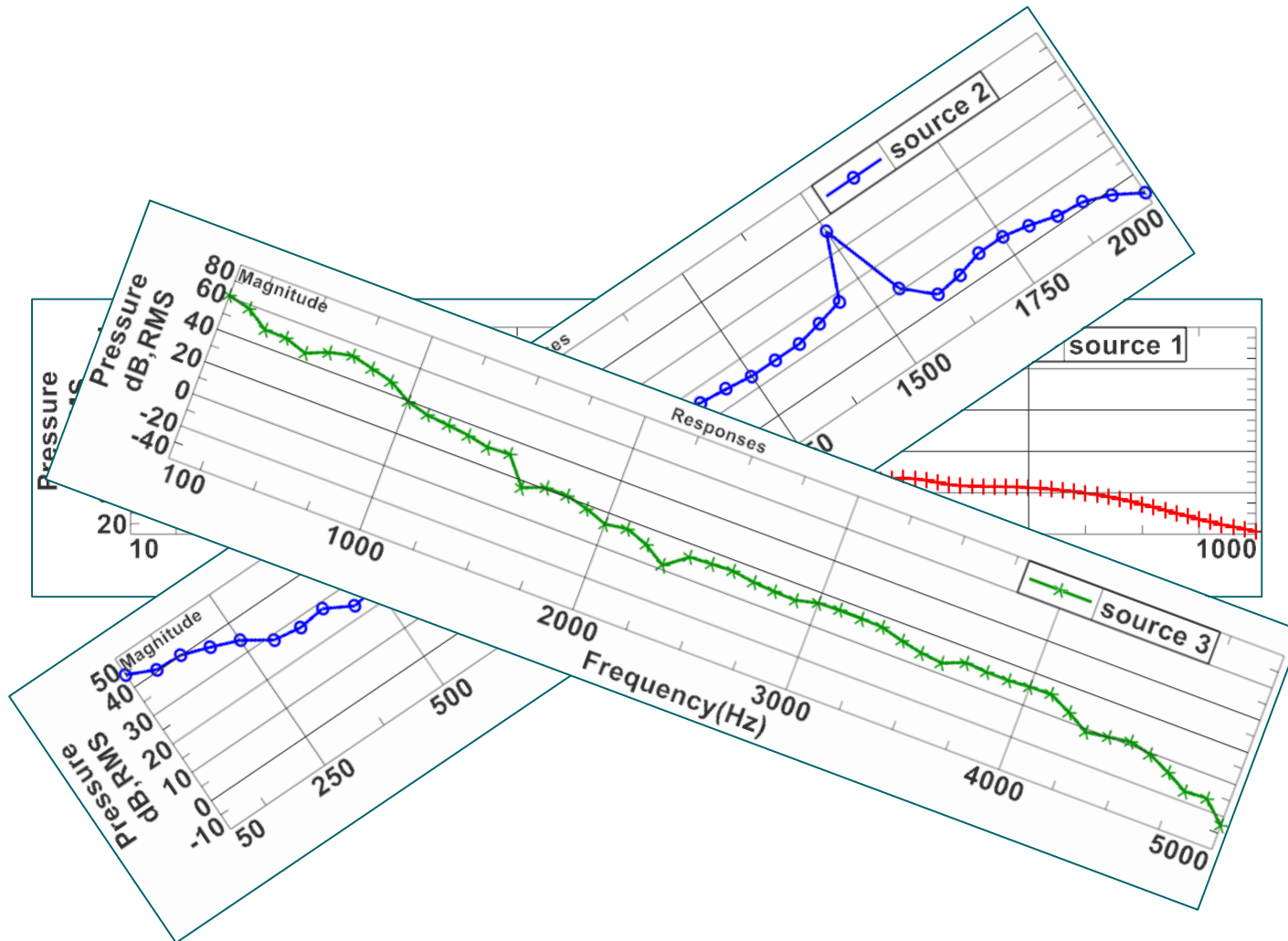
Why simulating flow-induced-noise?

Noise radiated by the internal combustion engine is not an issue for electric vehicles
the noise generated by other existing sources will be “heard” by the driver and passenger



Flow-induced-noise

Broadband characteristic of the acoustic response



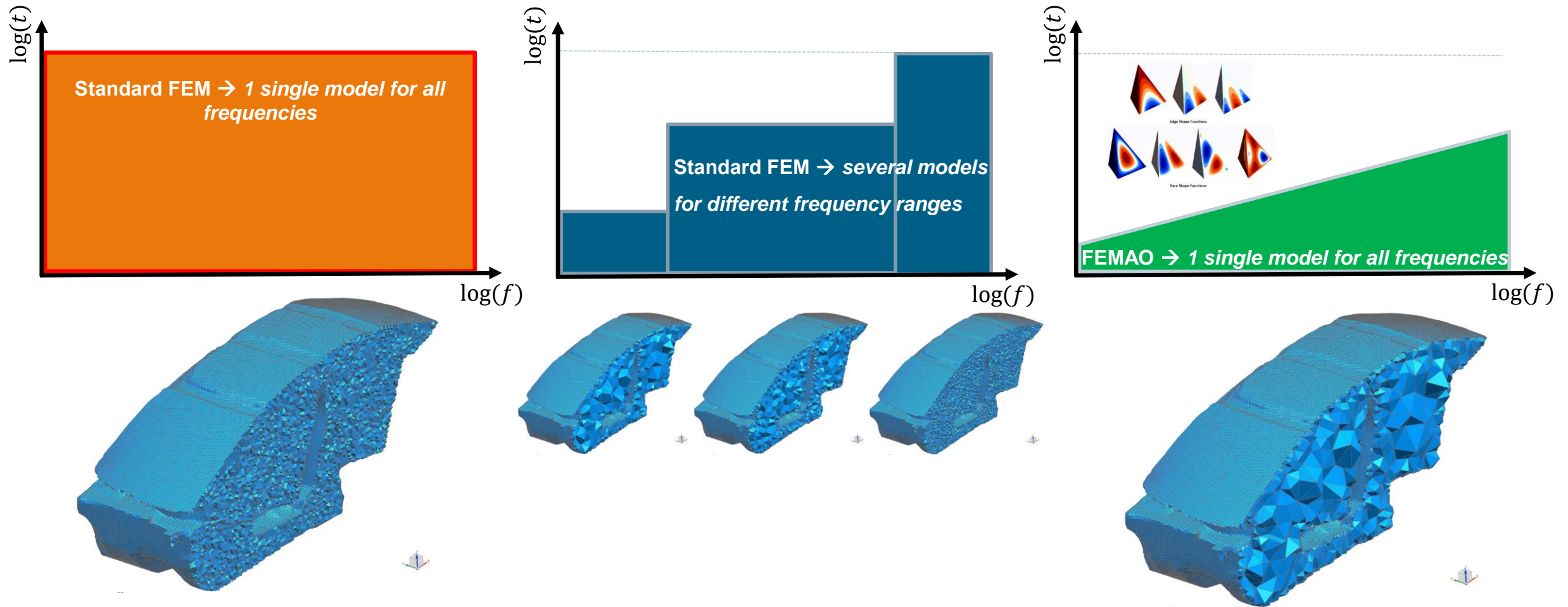
Random turbulent flow field around the source causing both **Tonal** and **Broadband** acoustic response

Requirement of an efficient solution of a multi-frequency problem

From lowest frequencies to higher frequencies of interest

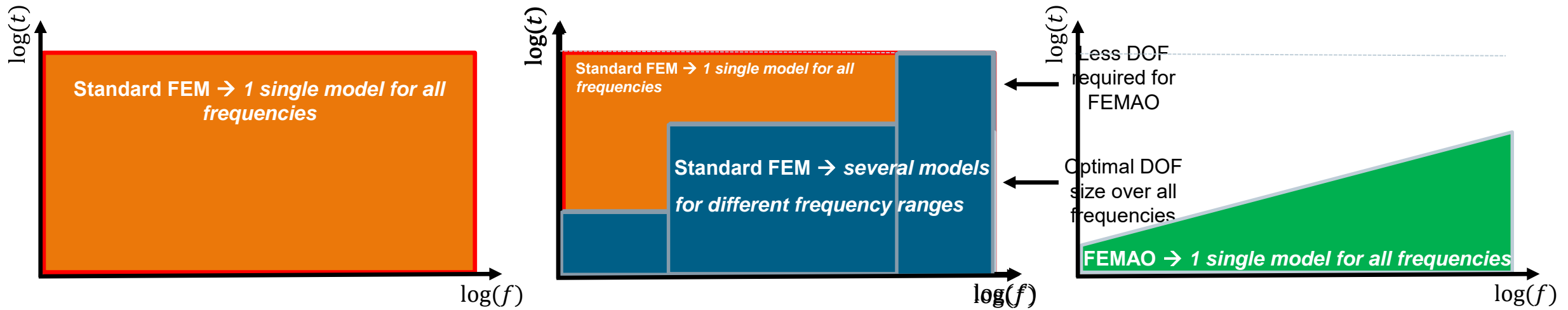
Simcenter 3D Acoustics – FEMAO

Alternative solutions

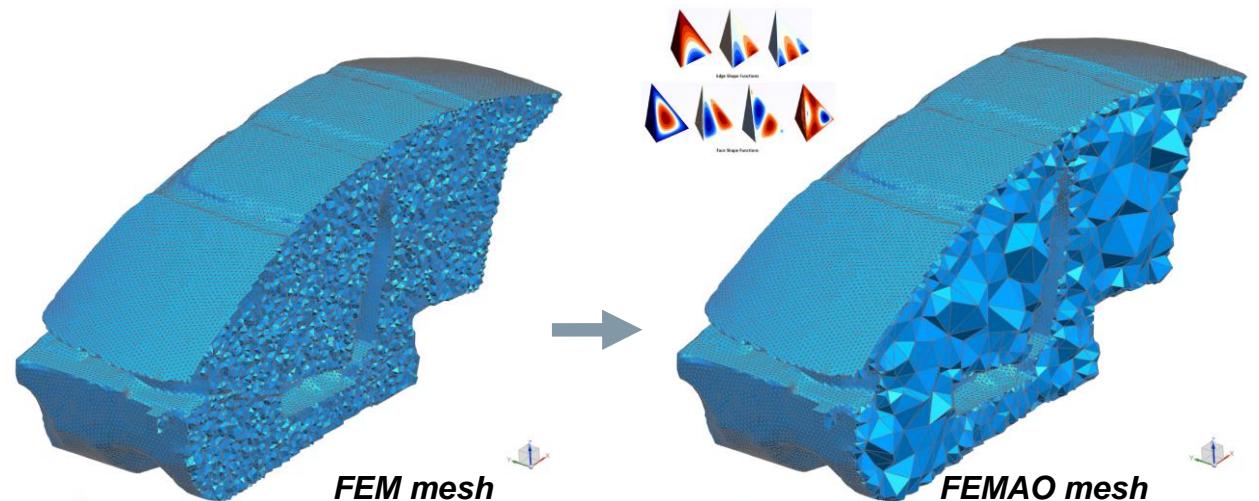


Simcenter 3D Acoustics – FEMAO

Benefits



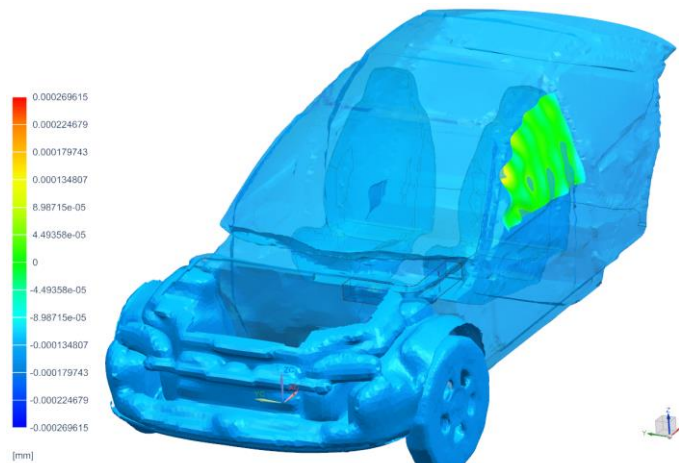
- Auto-adapting (f) fluid element order
- Leaner models in pre-processing
- Faster at lower frequencies
- More efficient at higher frequencies
- 2 to 10 times faster compared to standard FEM



The supremacy of lean FE models to solve flow-induced noise

Three flow-induced noise applications examples with FEMAO

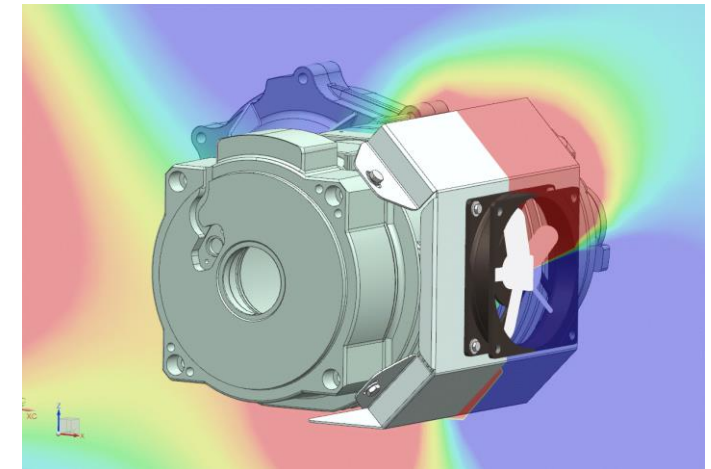
Windnoise



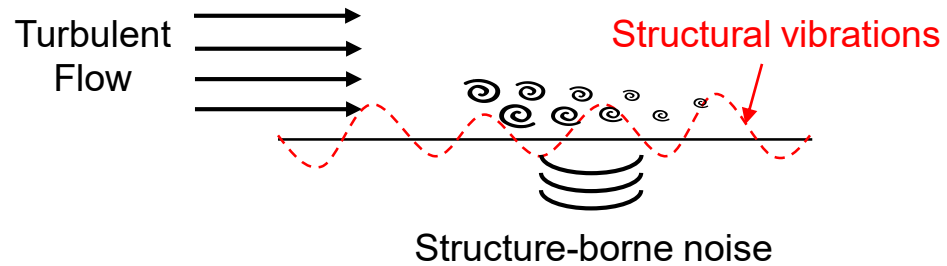
HVAC noise



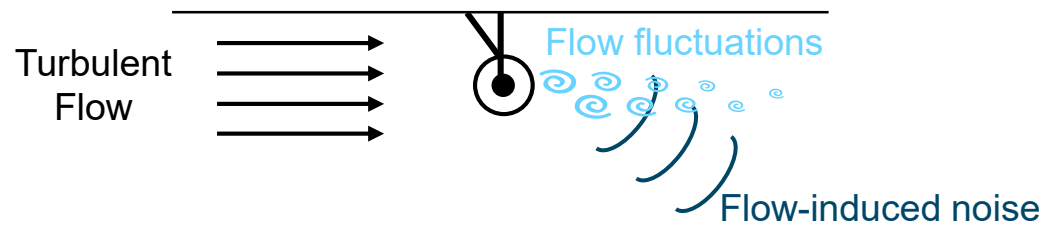
Fan noise



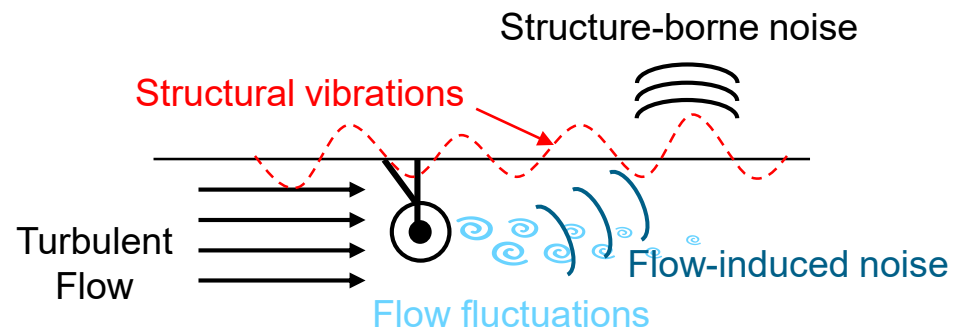
Acoustics: What happens in the presence of flow?



Flow-induced vibrations → Vibro-acoustics



Flow-induced noise → Aero-acoustics

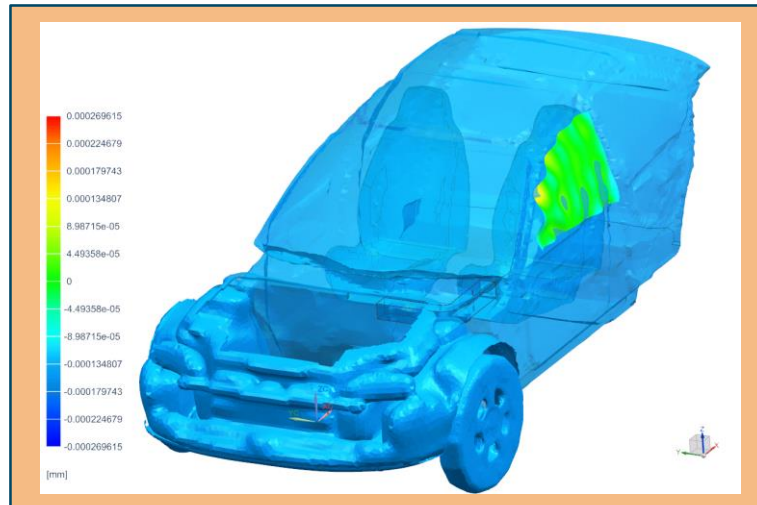


Flow-induced vibrations → Aero-vibro-acoustics

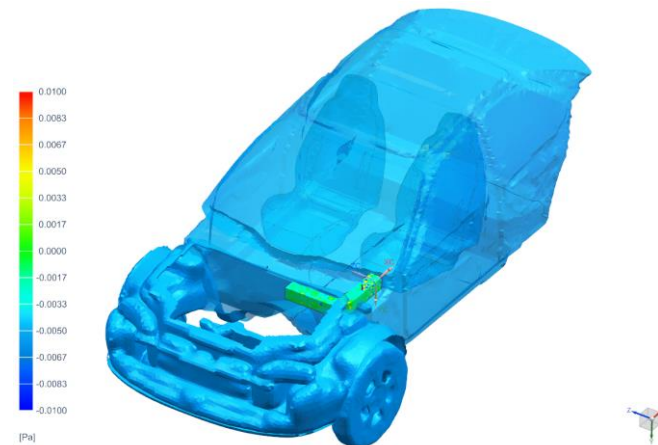
The supremacy of lean FE models to solve flow-induced noise

Three flow-induced noise applications examples with FEMAO

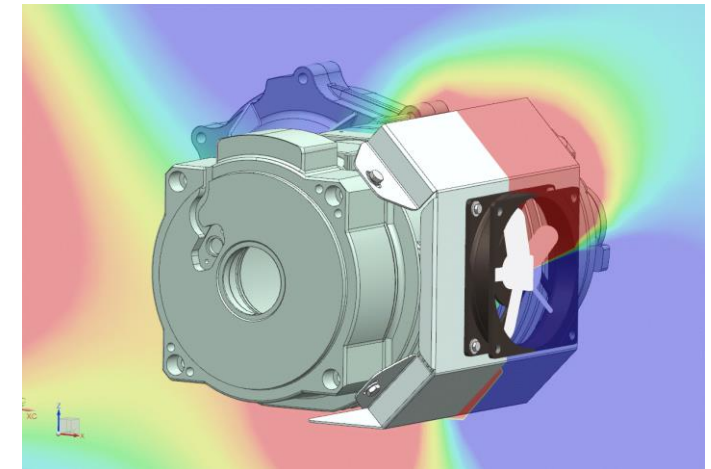
Windnoise



HVAC noise

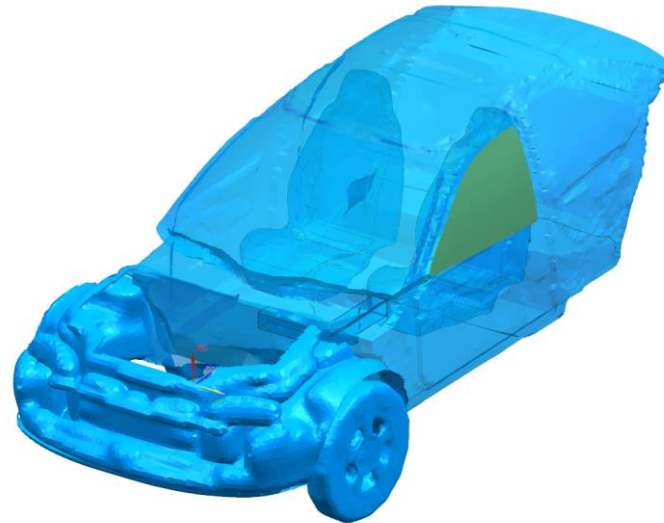
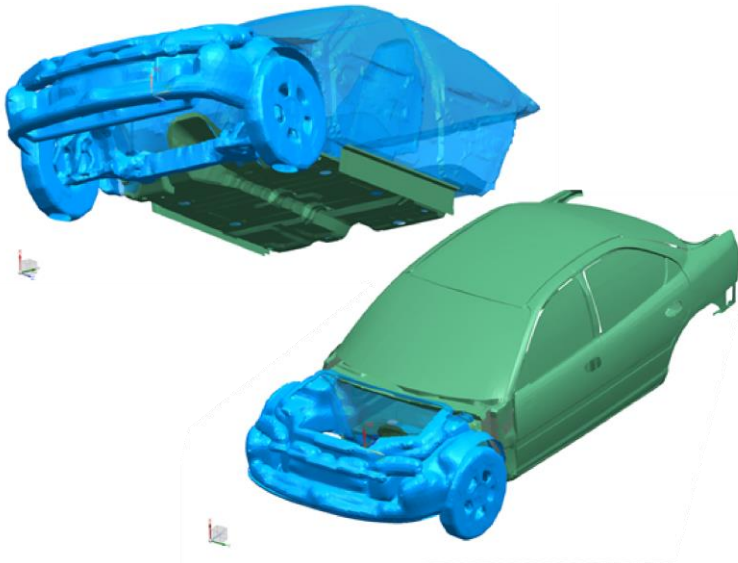


Fan noise



Cabin Wind Noise – Aero-Vibro-Acoustics

Which frequency range? Which loading?



<p>Low-frequency wind noise $f < 500$ Hz Underbody and green house</p>	<p>High-frequency wind noise $1000 \text{ Hz} < f < 5000$ Hz Side window and/or windshield</p>	<p>High-frequency wind noise $500 \text{ Hz} < f$ Underbody and green house</p>
<p>Structure: Simcenter Nastran FEM Acoustics: Simcenter Nastran FEM/FEMAO</p>	<p>Structure: Simcenter Nastran FEM Acoustics: Simcenter Nastran FEMAO</p>	<p>Virtual SEA+ / SEA+</p>
<p>Covered by FEM and FEMAO</p>		<p>Covered by SEA</p>

Windnoise simulation workflow

Aerodynamic field

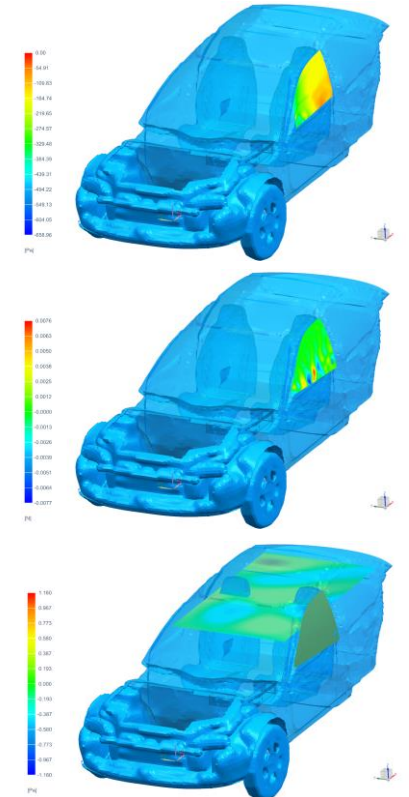
Starting from external aerodynamic loading on the CFD mesh boundaries

Load Preparation

Preparation of wind loads for the vibro-acoustic model via advanced mapping

Vibro-acoustic solution

Vibro-acoustic computation of the side-window and car interior using wind loads



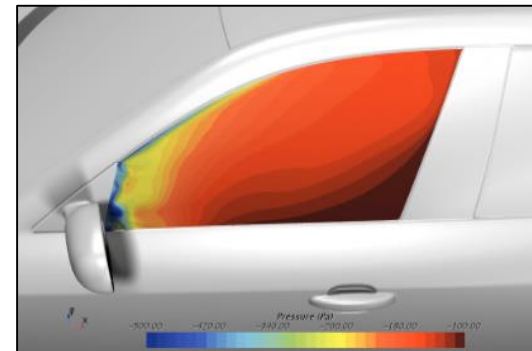
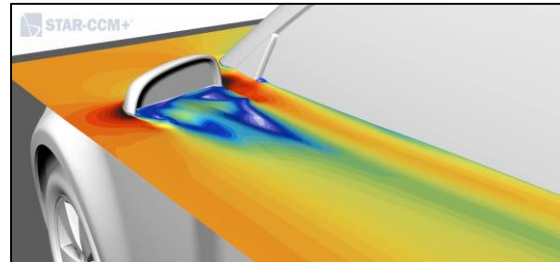
Windnoise simulation workflow

Aerodynamic field

Load Preparation

Vibro-acoustic solution

External aerodynamic field around the car



Solve exterior aerodynamics of the vehicle in Simcenter STAR-CCM+

Export aerodynamic and acoustic pressure on side window in CGNS

Name	Type	Size
Sidewindow_01001.cgns	CGNS File	2,928 KB
Sidewindow_01002.cgns	CGNS File	2,928 KB
Sidewindow_01003.cgns	CGNS File	2,928 KB
Sidewindow_01004.cgns	CGNS File	2,928 KB
Sidewindow_01005.cgns	CGNS File	2,928 KB
Sidewindow_01006.cgns	CGNS File	2,928 KB

Windnoise simulation workflow

Aerodynamic field

Compute exterior aerodynamics accurately

Load Preparation

Vibro-acoustic solution

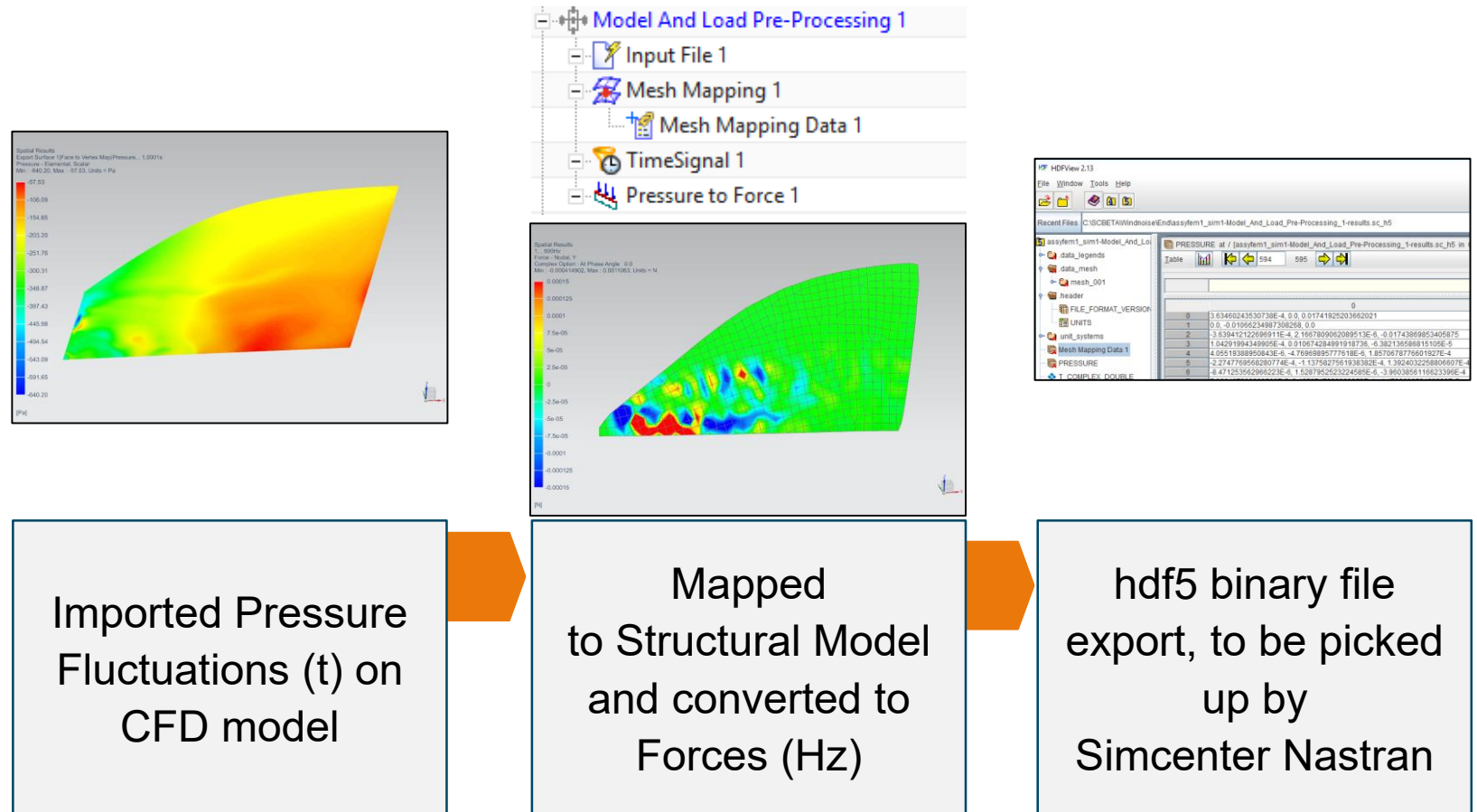
Windnoise simulation workflow

Aerodynamic field

Load Preparation

Vibro-acoustic solution

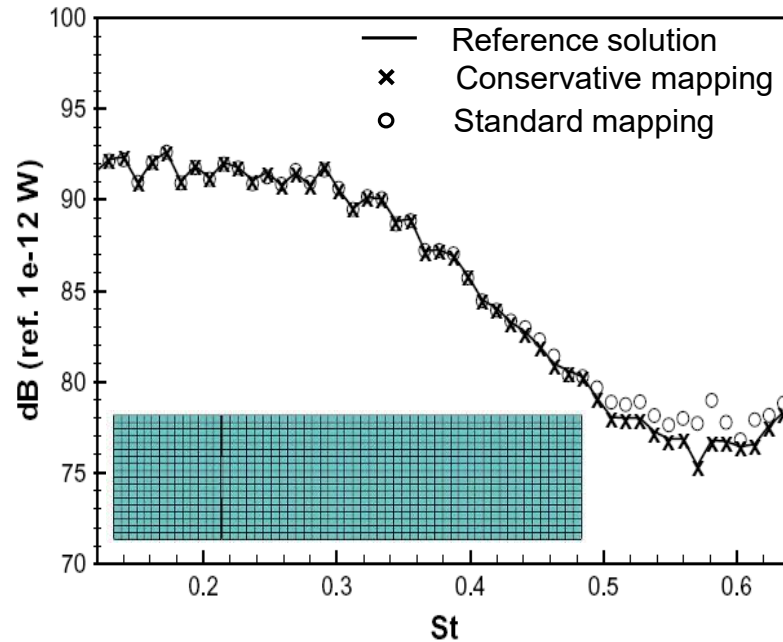
Load preparation for the vibro-acoustic simulation



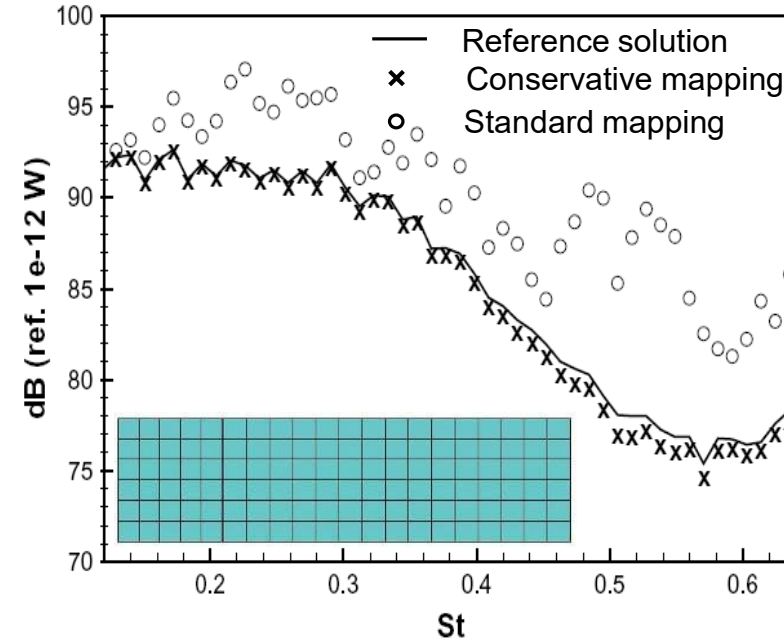
Conservative mapping

Effect of mapping on radiated acoustic power

Acoustic mesh has ~7 times fewer elements than CFD mesh



Acoustic mesh has ~72 times fewer elements than CFD mesh



Conservative mesh mapping algorithm :

- Acoustic mesh can be much coarser
- Performance improvement for solving the acoustic model
- Better accuracy of the predicted acoustic radiation

Windnoise simulation workflow

Aerodynamic field

Compute exterior aerodynamics accurately

Load Preparation

Prepare external loads smoothly for the vibro-acoustic model

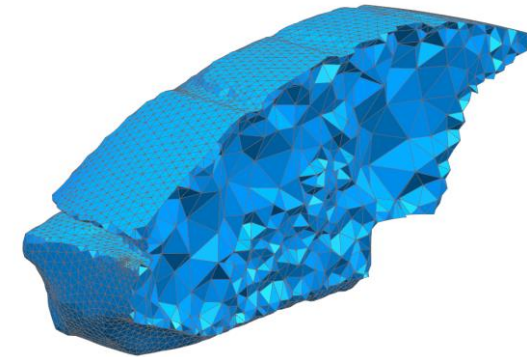
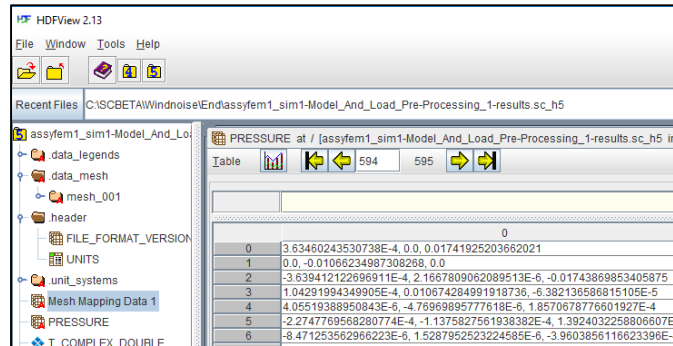
Vibro-acoustic solution

Aerodynamic field

Load Preparation

Vibro-acoustic solution

FEMAO: State-of-art FE solver with Adaptive Element Order



ANALYSIS NUMBER 36 / 36 FREQUENCY = 2000.000 Hz

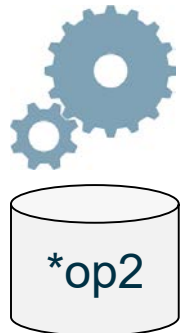
Time -- Delta: 0:00:00 (0.00) Total: 0:00:35 (35.93)

ADAPTIVE ORDER STATISTICS (in % of total volume)

1	2	3	4	5	6	7	8	9	10
0.20	12.79	34.14	28.50	19.30	4.72	0.35	0.00	0.00	0.00

User friendly link to hdf5 binary file to be picked up by Simcenter Nastran RLOADEX

Vibro-acoustic response in the cabin with FEMAO in Simcenter Nastran

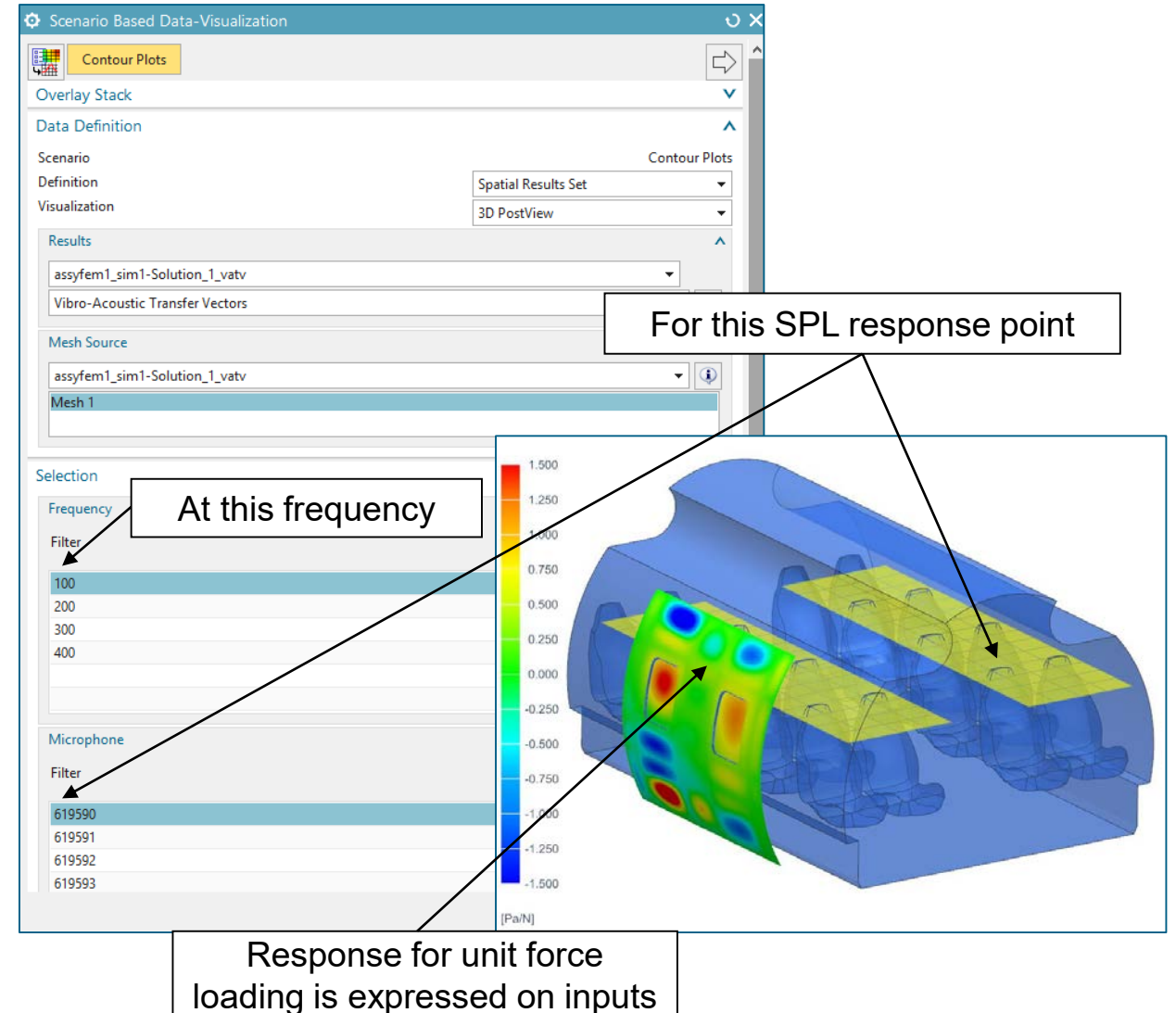


Vibro-Acoustic Transfer Vectors (VATV) For Faster Multi-Load Case Response Analysis

VATV = SPL response to unit surface loads ~ FRF
Computed using reciprocity principle

Key benefit

- No need to re-compute VATV as long as model remains the same
- Response is quickly computed for different loads:
 - TBL loads for aircraft panel x VATV
 - CFD loads on a car side window x VATV
 - Acoustic loads on car window from tailpipe x VATV



Windnoise simulation workflow

Aerodynamic field

Compute exterior aerodynamics accurately

Load Preparation

Prepare external loads smoothly for the vibro-acoustic model

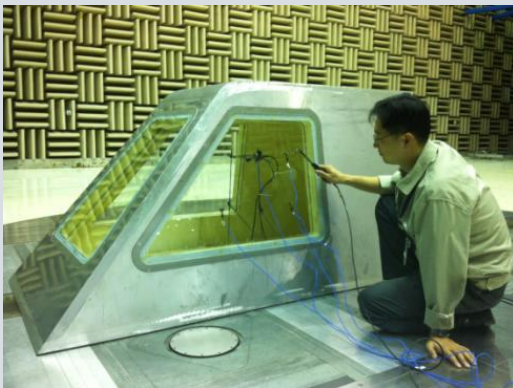
Vibro-acoustic solution


Efficient finite element computation using single coarse physical mesh for all frequencies of interest

Validation

Hyundai Motor Company simplified model

Simplified cabin from literature





inter.noise 2015

 SAN FRANCISCO CALIFORNIA USA

Wind noise simulation on Hyundai Simplified Model using multi-disciplinary CFD - Vibro-acoustic approach

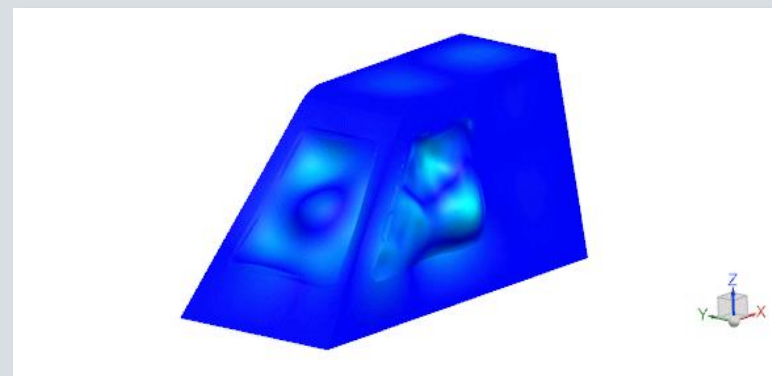
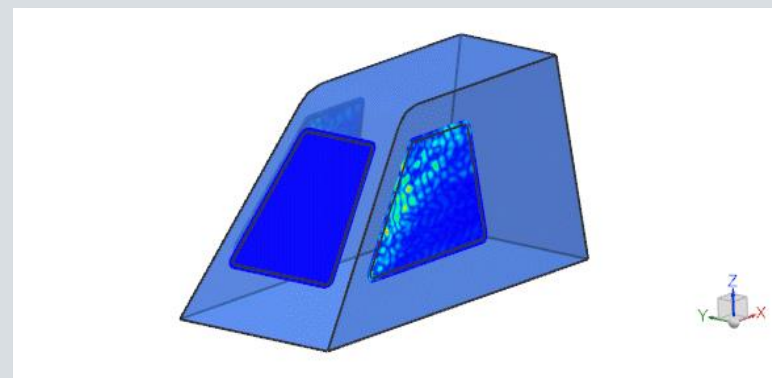
Korean Kucukocokun¹⁾
 Koen Vannier²⁾
 SIEMENS PLM Belgium
 Interleuvelaan 68, 3001 Leuven, Belgium

Ashok Khondge³⁾
 ANSYS India
 34/2 Rajiv Gandhi Infotech Park MIDC Hinjewadi, Pune, 411057, India

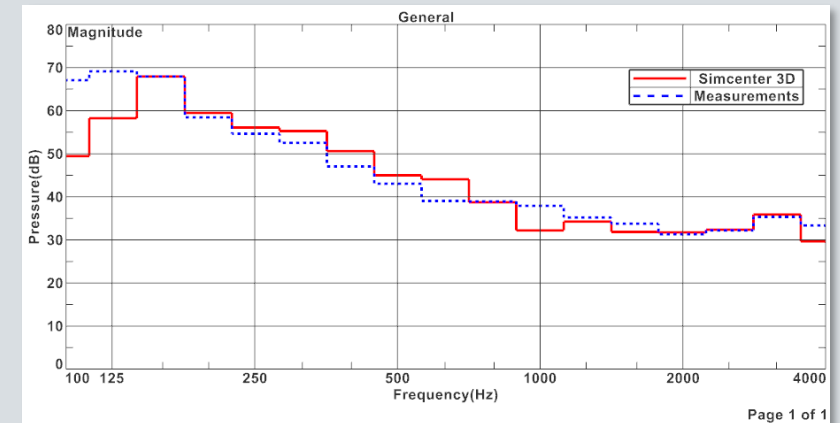
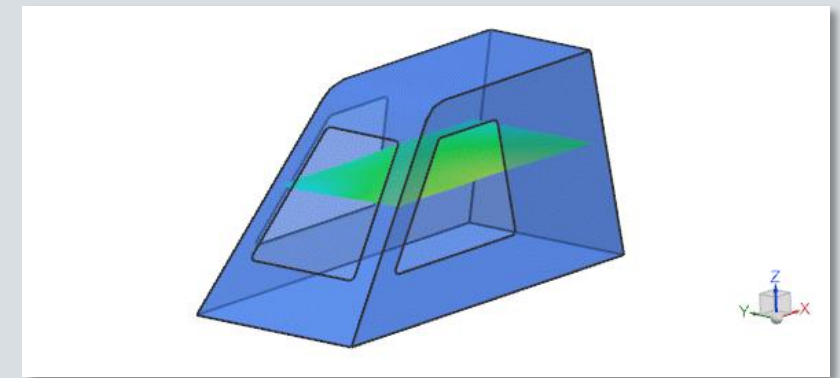
Jeongwon Lee⁴⁾
 ANSYS Korea
 22F City Air Tower 139-9, Samsung-dong, Kangnam-gu 135-973, Seoul, Korea

Sang Yeop Lee⁵⁾
 SIEMENS PLM Korea
 7th Fl., KOTTA Bldg., 37 Baumeo-ro37-gil, Seocho-gu, Seoul 137-888, Korea

Vibro-acoustic solution with Simcenter 3D



Comparing pressure results with measurements



Windnoise simulation workflow

Aerodynamic field

Compute exterior aerodynamics accurately

Load Preparation

Prepare external loads smoothly for the vibro-acoustic model

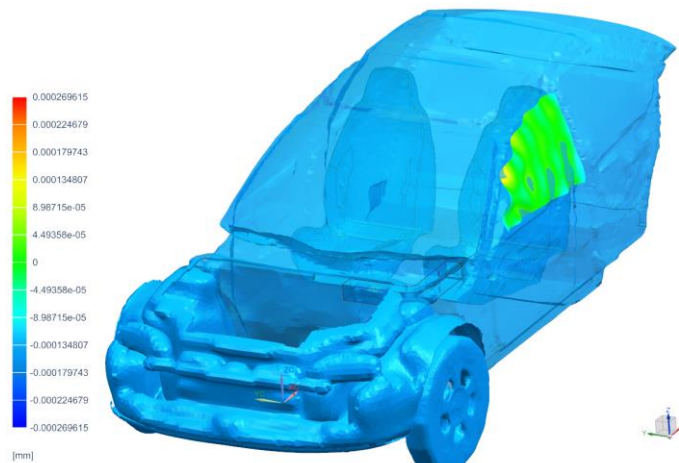
Vibro-acoustic solution

Efficient finite element computation using single coarse physical mesh for all frequencies of interest

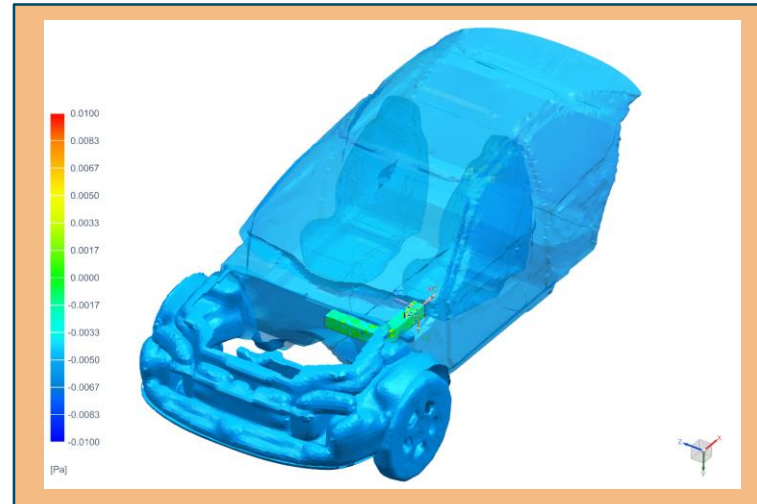
The supremacy of lean FE models to solve flow-induced noise

Three flow-induced noise applications examples with FEMAO

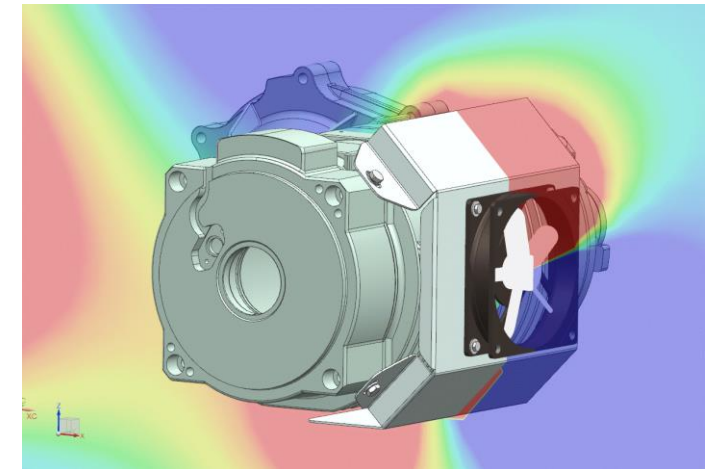
Windnoise



HVAC noise

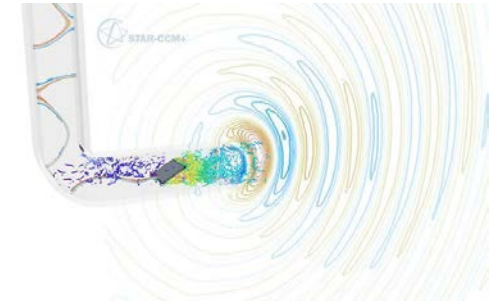
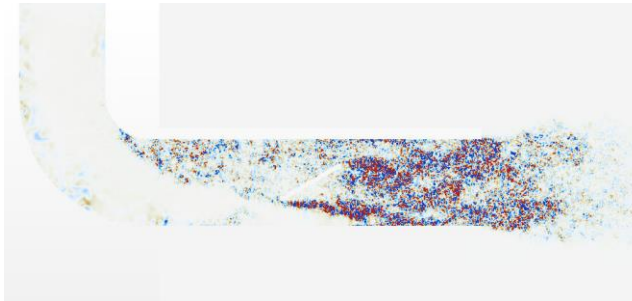
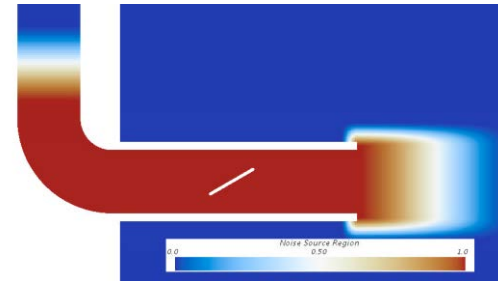
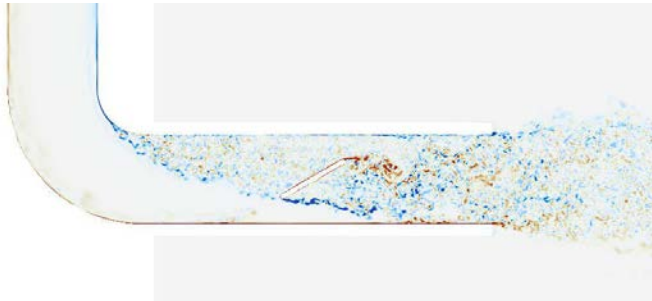


Fan noise



Simcenter STAR-CCM+

Acoustic Perturbation Equation (APE) Solution



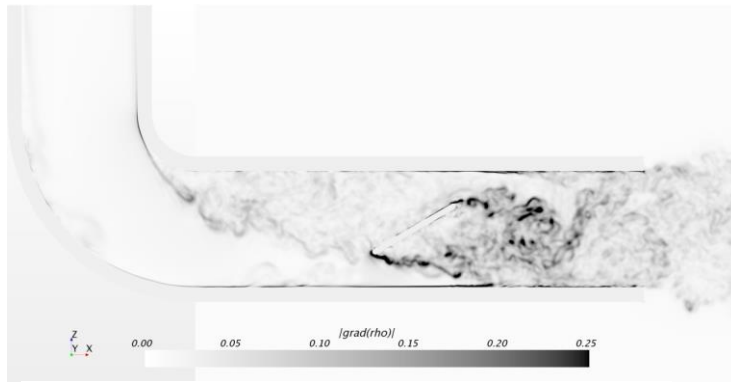
Calculate flow field

Specify a source region where noise sources are calculated

Calculate the noise sources

Use APE to calculate the sound waves

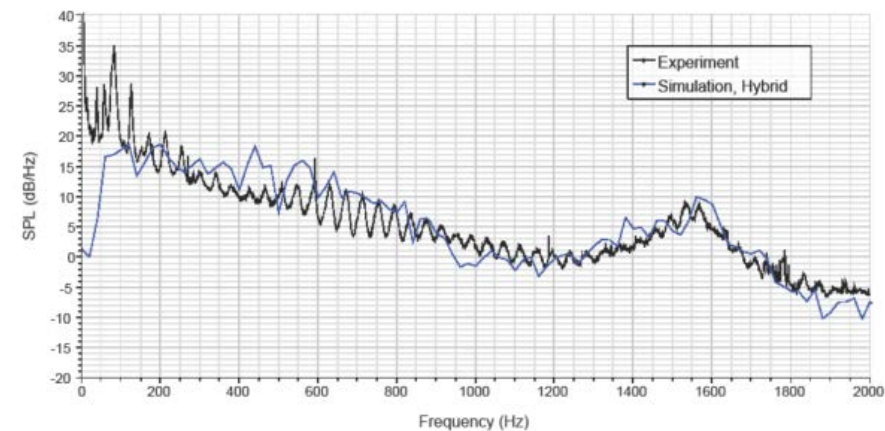
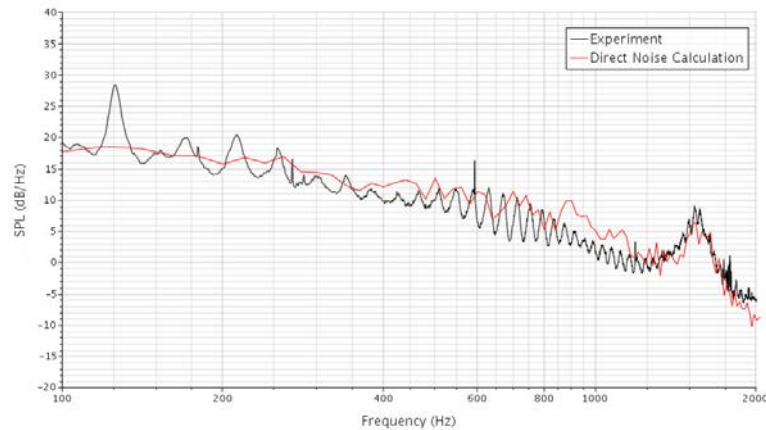
Simcenter STAR-CCM+ approaches Duct Elbow



Direct Noise Calculation



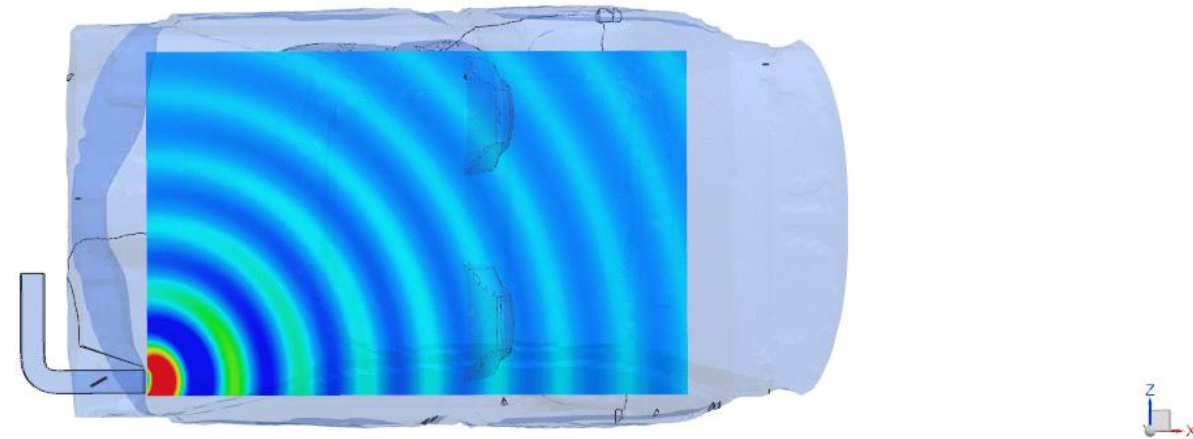
Hybrid (Acoustic Perturbation Equation)



HVAC Noise Simulations

Component level free-field propagation

Acoustic wave propagation from HVAC outlet
in free-field



Acoustic wave propagation from HVAC outlet
inside cabin with absorbing surfaces such as
seats, carpet and roof

?

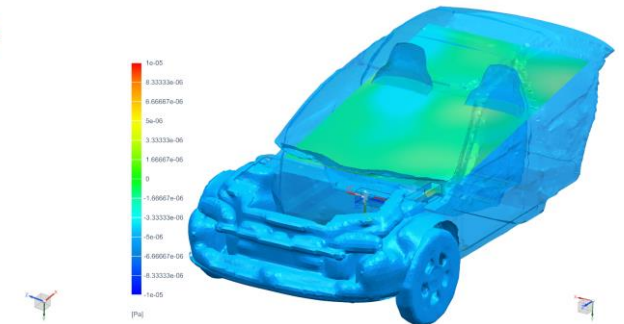
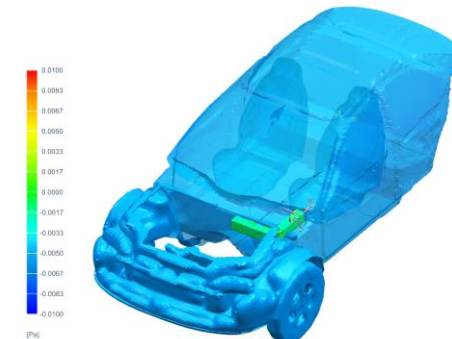
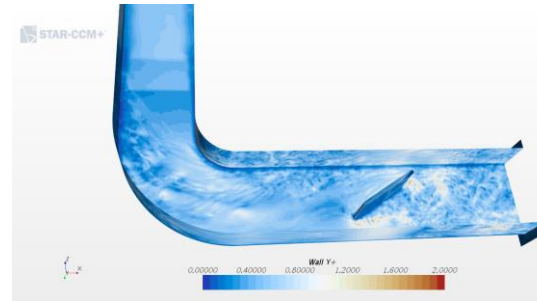
Aeroacoustics hybrid simulation workflow

Aerodynamic load preparation

Aeroacoustic source modeling

Acoustic propagation

From CFD output files to propagation towards driver's ear

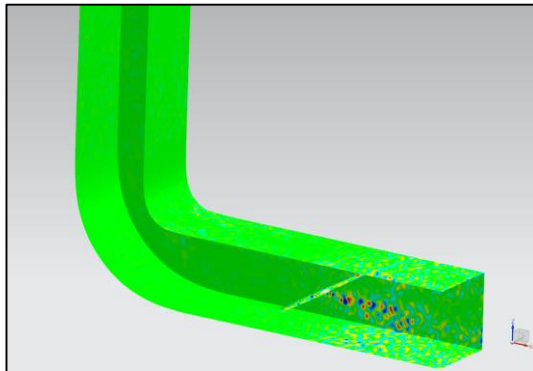


Turbulent flow field in the duct with Simcenter STAR-CCM+

Load and Source Preparation for aeroacoustics simulation with Simcenter 3D

Solution of the acoustics field in the car cabin with Simcenter Nastran

Generation of advanced aeroacoustics sources



Aerodynamic pressure loading on the HVAC components

	0	1	2	3	4	5	6
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T COMPLEX DOUBLE	4.05519388950843E-6, -4.76969895777618E-6, 1.8570678776601927E-4						
	-2.2747769568280774E-4, -1.1375827561938382E-4, 1.3924032258806607E-4						
	-8.471253562966223E-6, 1.5287952523224585E-6, -3.9603856116623396E-4						

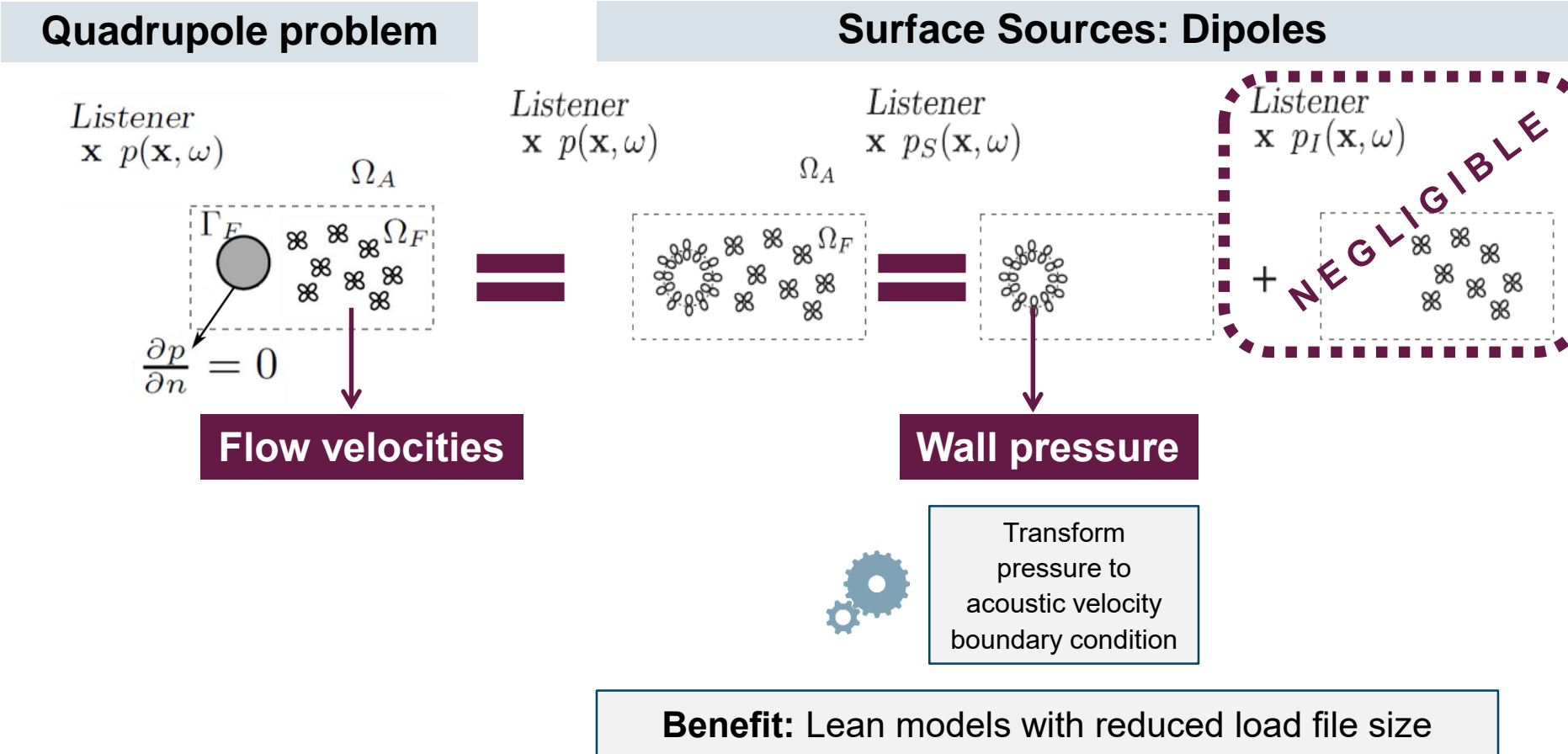
Easy link to the hdf5 load file to be picked up by Simcenter Nastran ACSP02



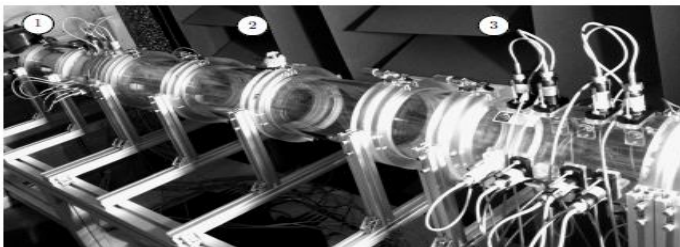
Transform pressure to acoustic velocity boundary condition

Advanced aeroacoustic sources for HVAC duct components

Scattered field of Quadrupole sources by the surfaces is equivalent to Dipole radiation for low-Mach Number flows



Cases description



Low average Mach number (around $M=0.07$)
 $D=0.150\text{m}$, $d=0.116\text{m}$, thickness 0.008m

AIAA 2016-2796

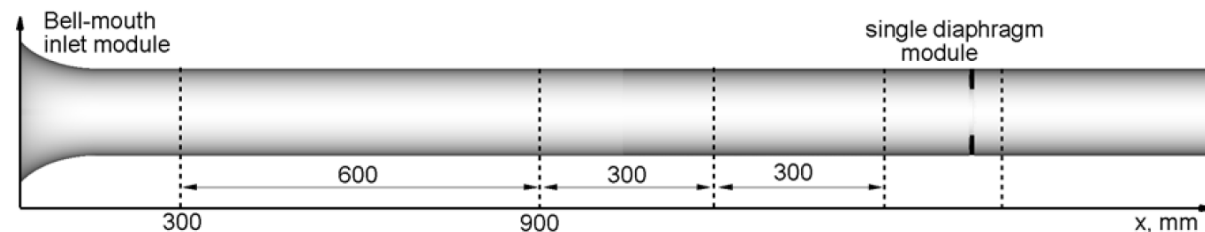
Hybrid aeroacoustic computations for flows in ducts with single and tandem diaphragms

P. Martínez-Lera*, K. Kucukcoskun†, M. Tournour‡
Siemens Industry Software NV, 3001 Leuven, Belgium

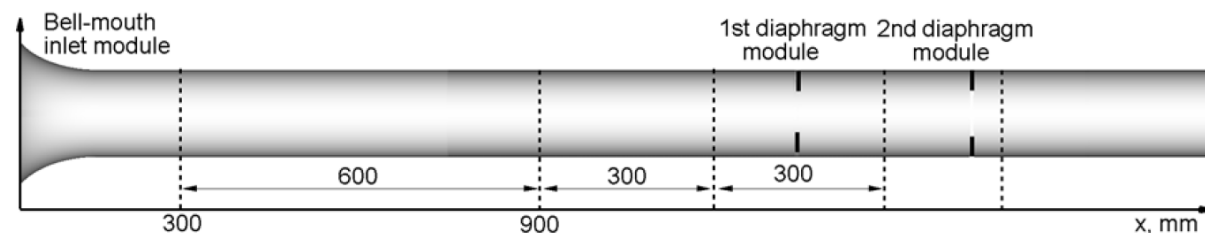
M. Shur§, A. Travin¶
Saint-Petersburg Polytechnic University and New Technologies & Services (NTS), Saint-Petersburg, 195220, Russia

This paper presents the results of hybrid aeroacoustics computations of the sound induced by the turbulent flow inside ducts with single and tandem diaphragms at low Mach numbers. The aeroacoustic sources are based on compressible flow data obtained with an Improved Delayed Detached Eddy Simulation method. The source models are either based on flow wall pressure, which is used to define equivalent acoustic boundary conditions, or on flow velocity fluctuations, which are used to define equivalent quadrupole sources. Several implementations of the source models are discussed in the context of a high-order finite element approach for acoustics. The acoustic results of the hybrid approach are compared to the results provided directly by the compressible flow computations, as well as to available experimental measurements.

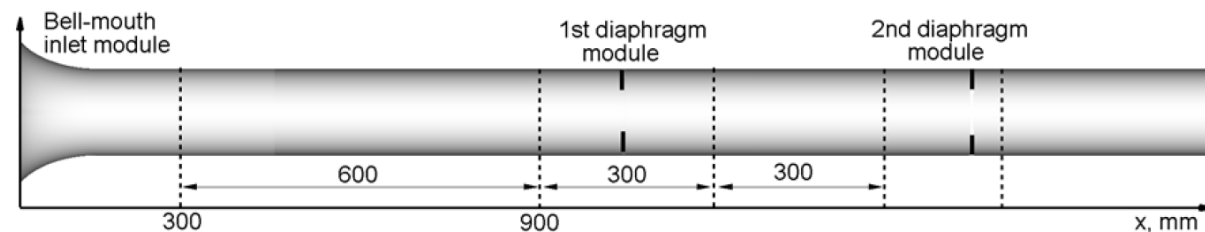
Single diaphragm



Tandem diaphragms (separation 2D)

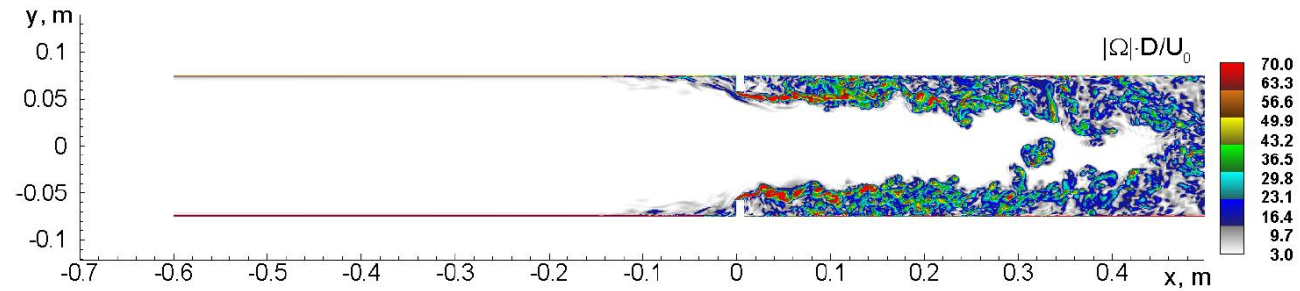


Tandem diaphragms (separation 4D)

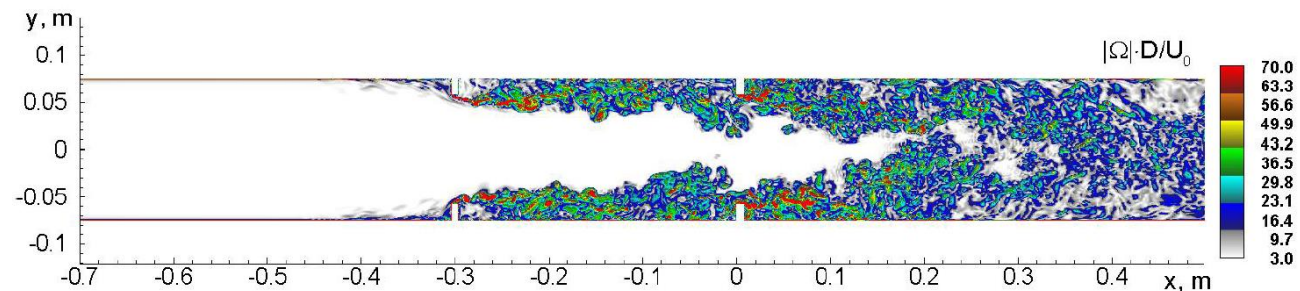


CFD: Snapshots of vorticity

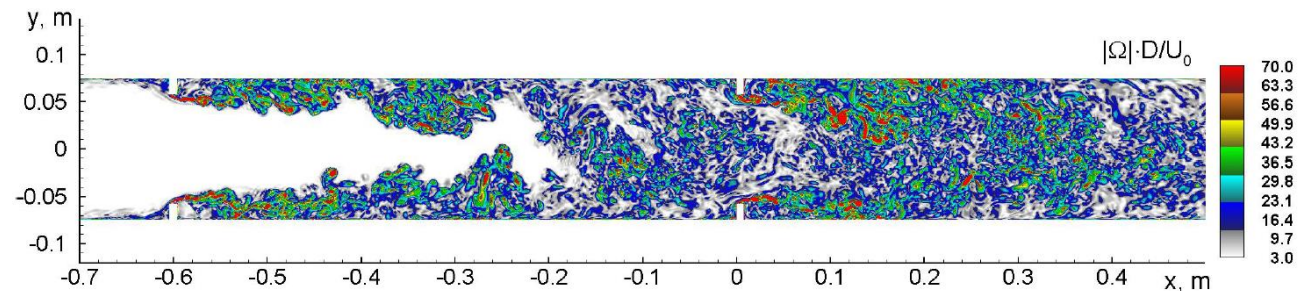
Single
diaphragm



Tandem
diaphragms
2D separation

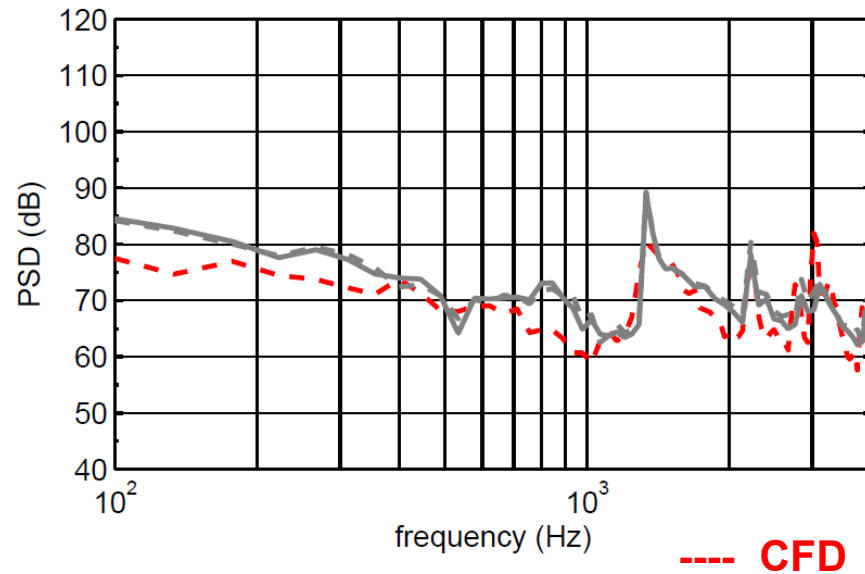


Tandem
diaphragms
4D separation

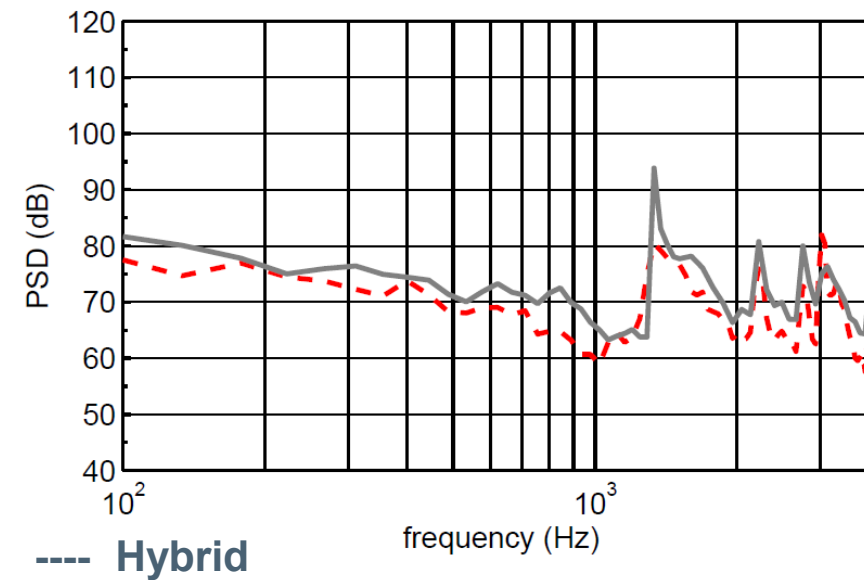


Single diaphragm: Acoustic prediction with quadrupole sources

Lighthill's analogy (no mean flow)



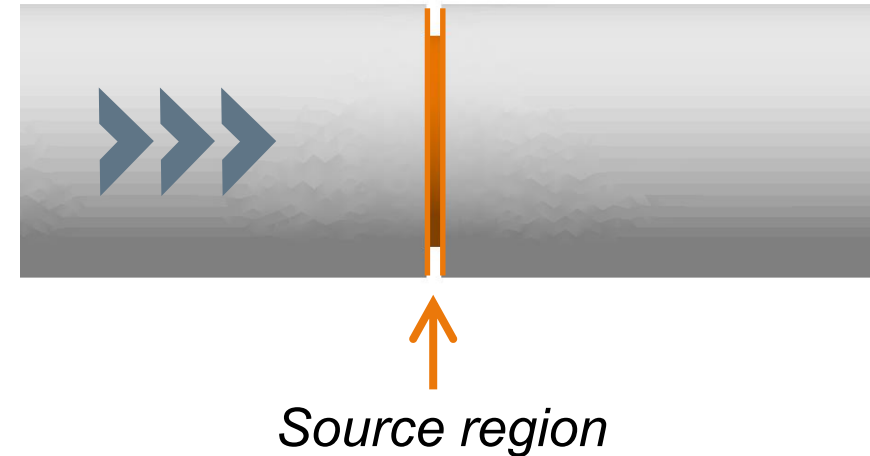
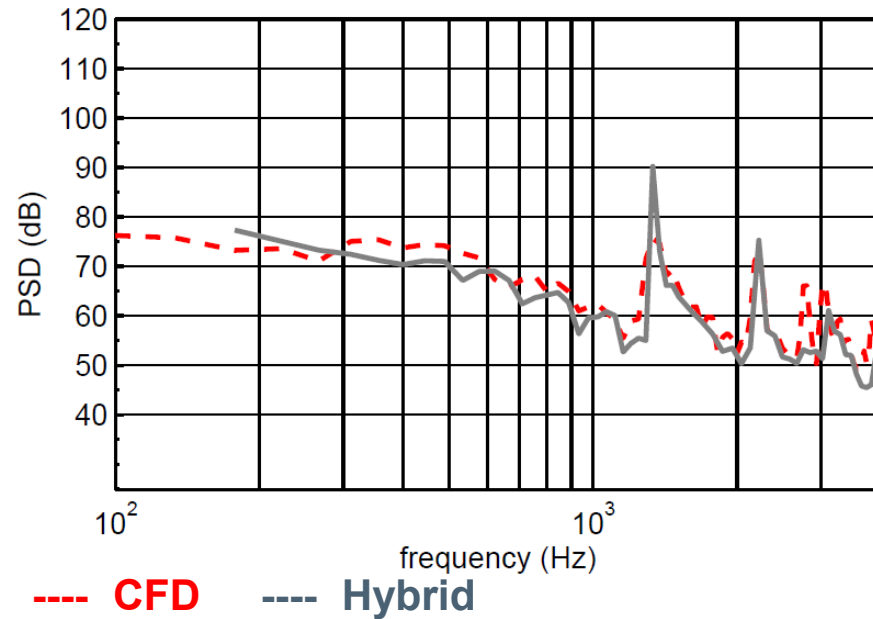
Vortex sound theory (mean flow)



Source region

Single diaphragm: Acoustic prediction with dipole sources

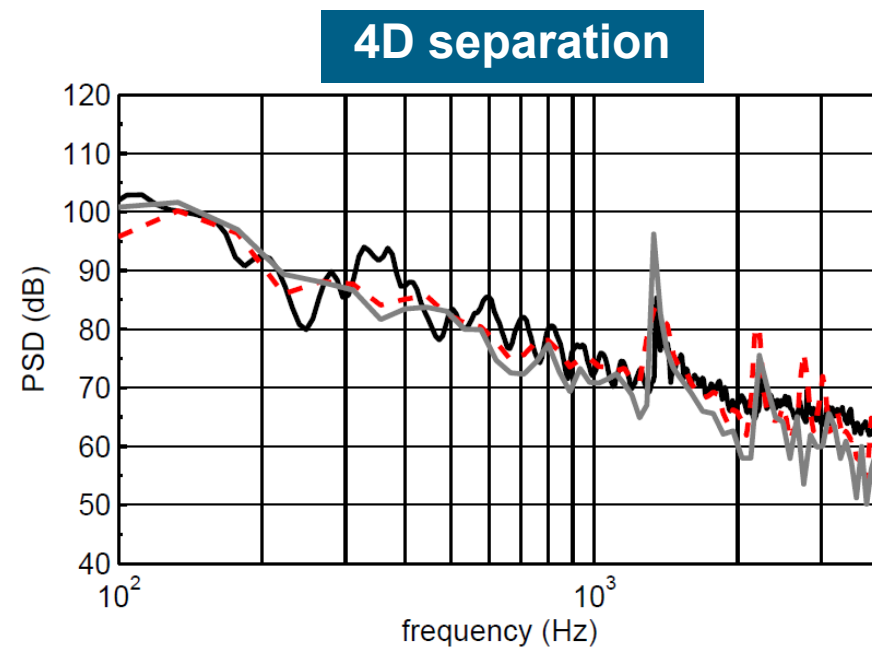
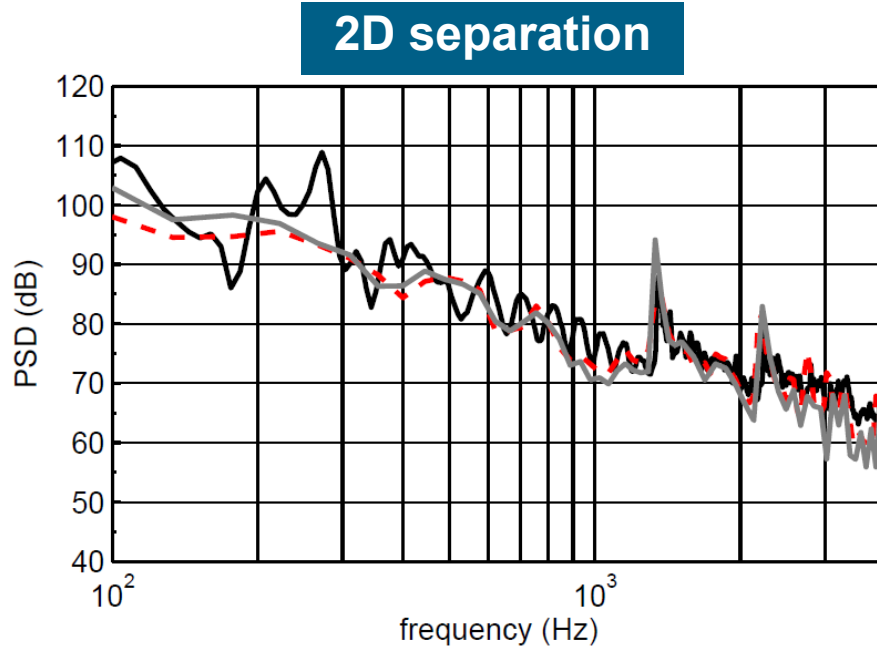
Dipole Sources



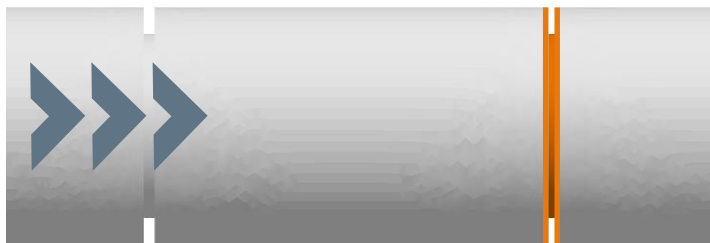
**Dipole sources on diaphragm surface
(dominant source of sound)**

Formulation can be applied to incompressible CFD input for similar low-Mach Number applications

Tandem diaphragms: Acoustic prediction with dipole sources



--- CFD --- Hybrid --- Experimental



Source region

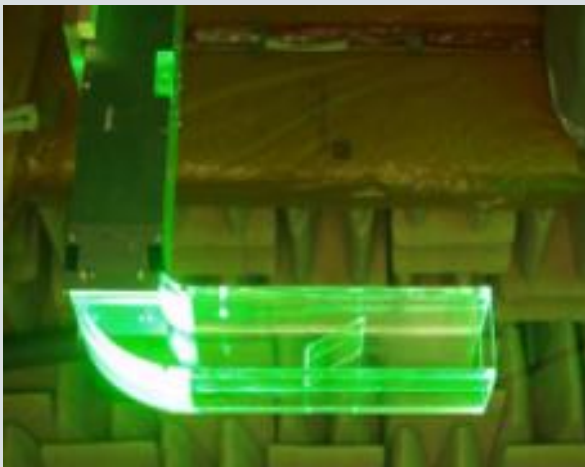
**Dipole sources on downstream diaphragm surface
(dominant source of sound)**

Formulation can be applied to incompressible CFD input
for similar low-Mach Number applications

HVAC Noise Simulations

Validation with academic model

Simplified HVAC from literature



2008-2902

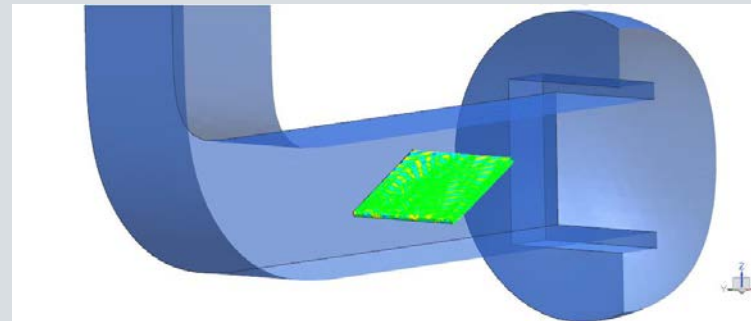
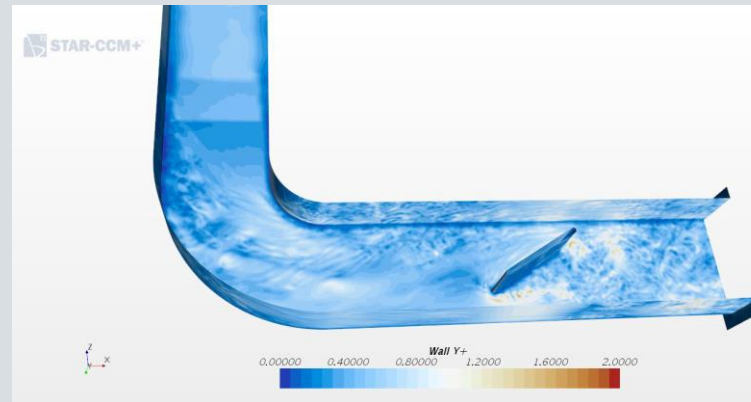
29th AIAA Aeroacoustics Conference, May 5-7 2008, Vancouver B.C.

Numerical and Experimental Investigations of the Noise Generated by a Flap in a Simplified HVAC Duct

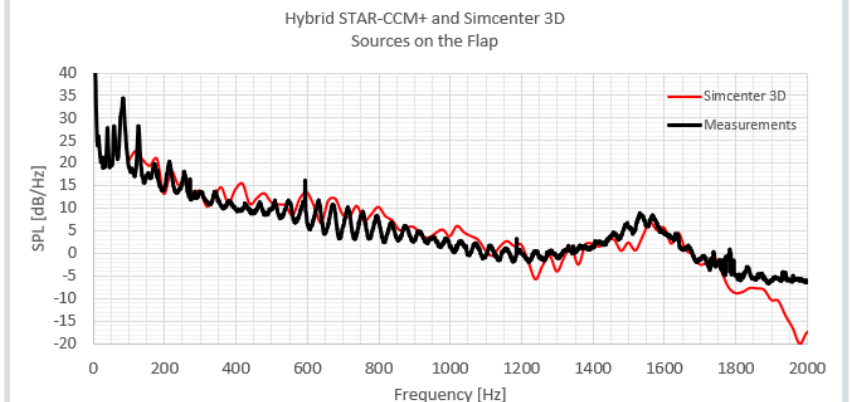
Anke Jäger¹, Friedhelm Decker¹, Michael Hartmann²,
Moni Islam³, Timo Lemke⁴, Jörg Ocker⁴, Volker Schwarz¹, Frank Ullrich⁵,
Berni Crouse⁶, Gana Balasubramanian⁷, Fred Mendonca⁷ and Roger Drobietz⁸

- ¹ Daimler AG, HPC X715, D-71059 Sindelfingen, Germany
- ² Volkswagen AG, Letterbox 1777, D-38436 Wolfsburg, Germany
- ³ Audi AG, Wind-Tunnel Center, D-85045 Ingolstadt, Germany
- ⁴ Dr.-Ing. h.c. F. Porsche AG, D-71286 Weissach, Germany
- ⁵ BMW AG, Dept. EG-42, D-80788 Munich, Germany
- ⁶ Exa Corporation, 150 North Hill Drive, Brisbane, CA 94005, USA
- ⁷ CD-adapco UK, 200 Shepherds Bush Road, London W6 7NL, United Kingdom
- ⁸ EADS Deutschland GmbH, Innovation Works, D-81663 Munich, Germany

Coupling Simcenter STAR-CCM+ with Simcenter 3D



Comparison of simulation results with measurements



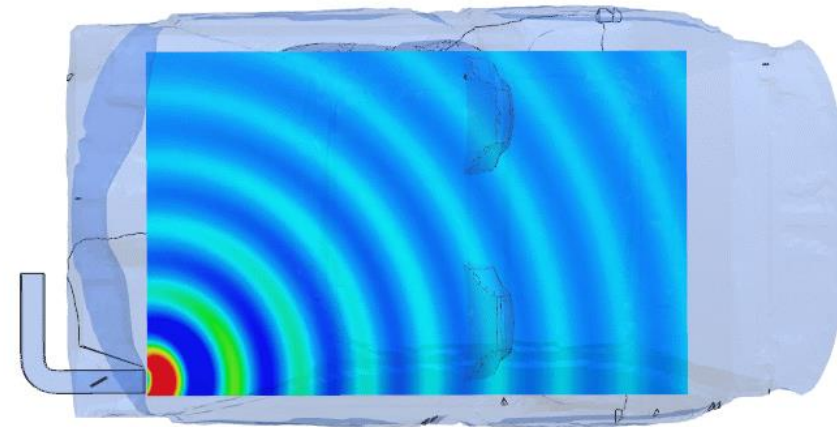
**Dipole sources on flap surface
(dominant source of sound)**

Formulation applied to
incompressible CFD input

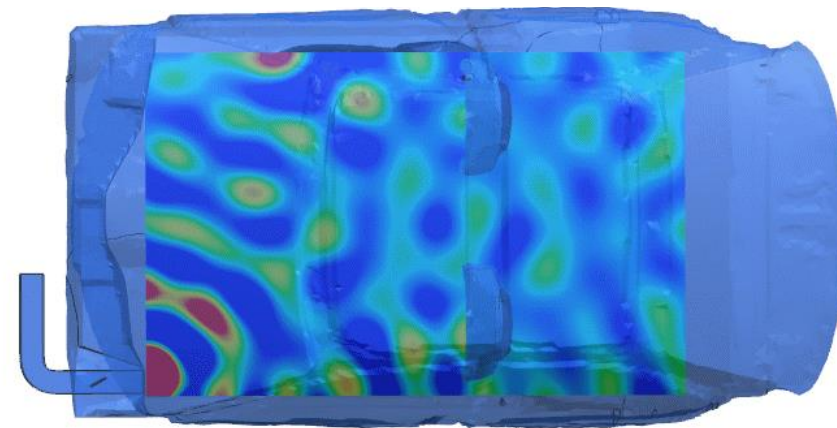
HVAC Noise Simulations

Propagation with cabin

Acoustic wave propagation from HVAC outlet
in free-field



Acoustic wave propagation from HVAC outlet
inside cabin with absorbing surfaces such as
seats, carpet and roof



Aeroacoustics simulation workflow



Aerodynamic load preparation

Prepare aerodynamic loads smoothly for the aeroacoustic problem

Aeroacoustic source modeling

Computation of the advanced aeroacoustics sources for stationary components

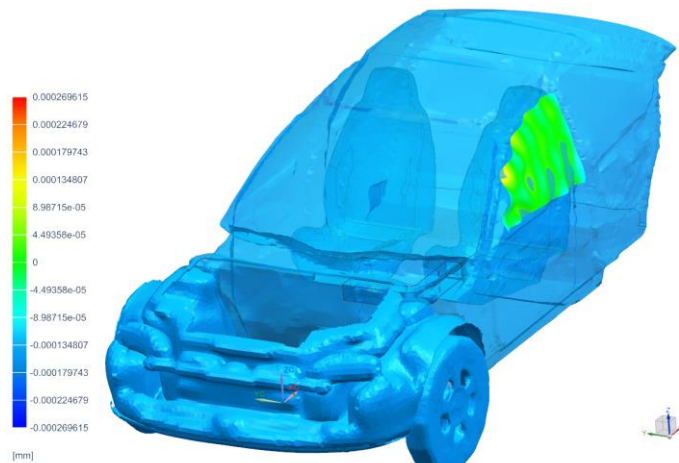
Acoustic propagation

Efficient finite element computation using single coarse physical mesh for all frequencies of interest

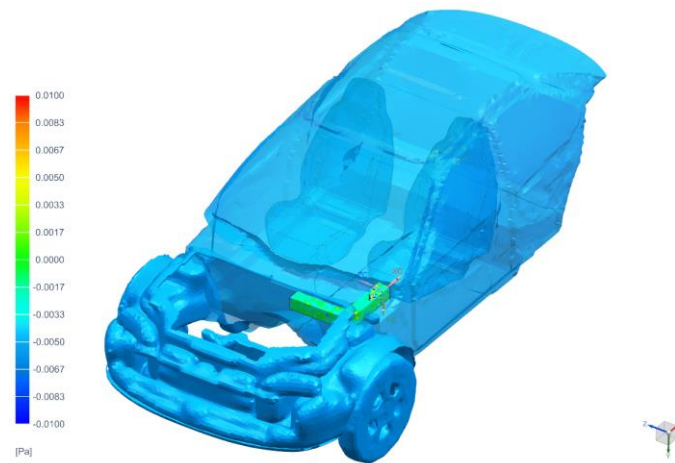
The supremacy of lean FE models to solve flow-induced noise

Three flow-induced noise applications examples with FEMAO

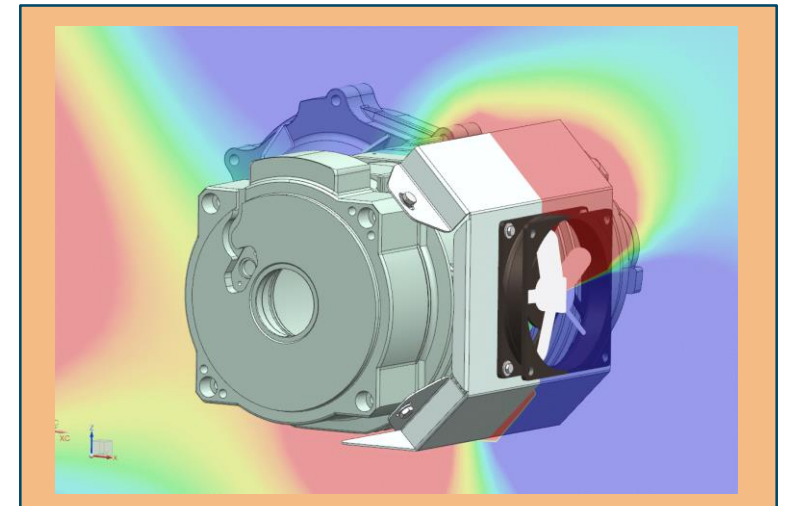
Windnoise



HVAC noise

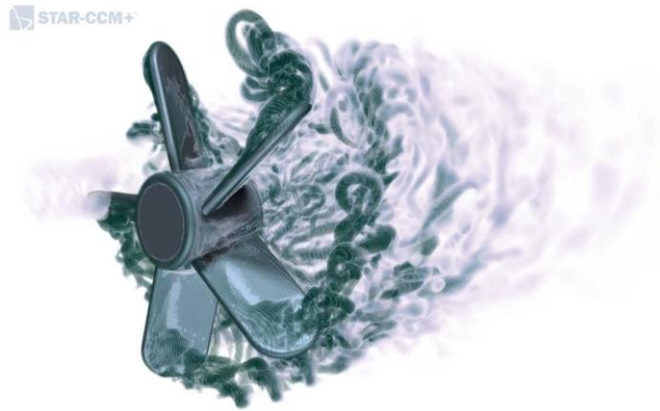


Fan noise

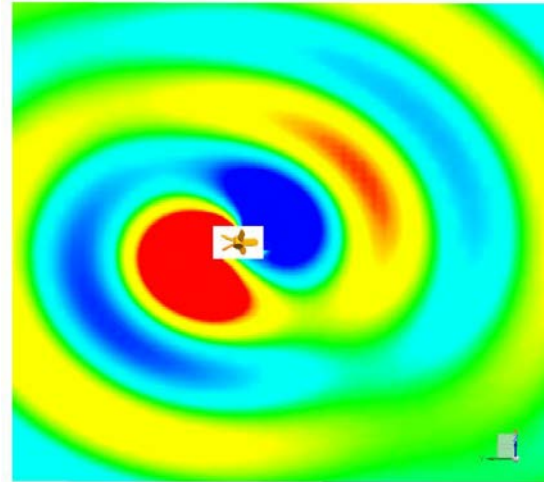


Cooling Fan Noise

Component level simulation



Compute unsteady flow field
around source region with
Simcenter STAR-CCM+

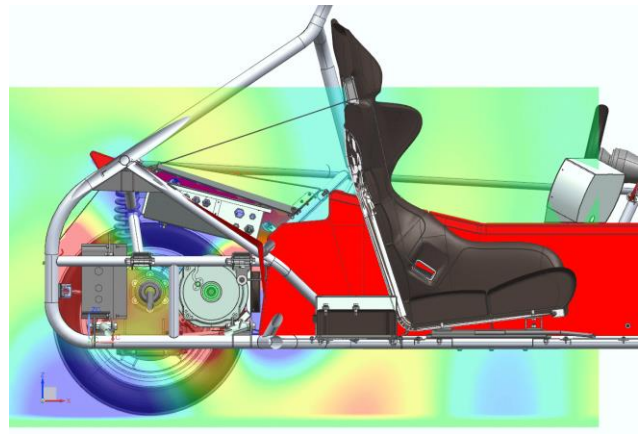
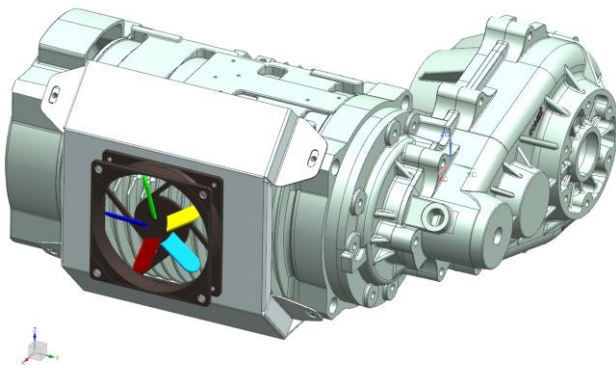
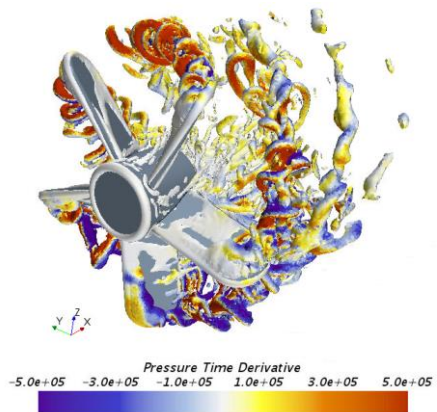


Compute free-field acoustic
propagation accurately



Installation effects,
reflective/absorbing
surface, infinite plates,
porous volumes in
propagation

From CFD output files to propagation towards driver's ear

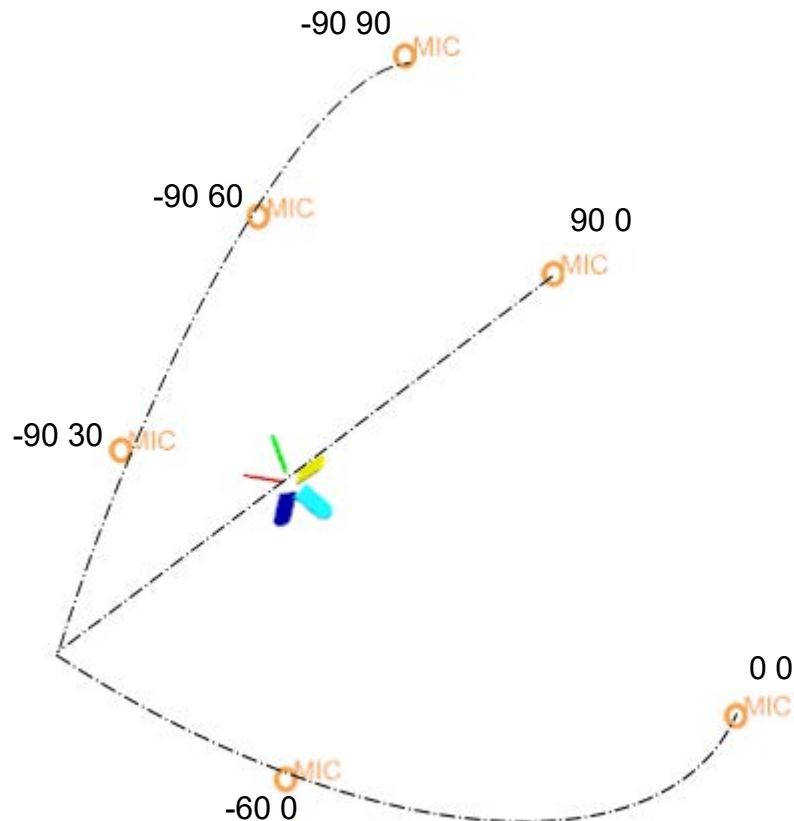


Turbulent flow field around the fan with Simcenter STAR-CCM+

Load and Source Preparation for aeroacoustics simulation with Simcenter 3D

Solution of the acoustic field towards the driver with Simcenter Nastran

Cooling Fan Noise Simulations in free-field with Simcenter STAR-CCM+ and Simcenter 3D



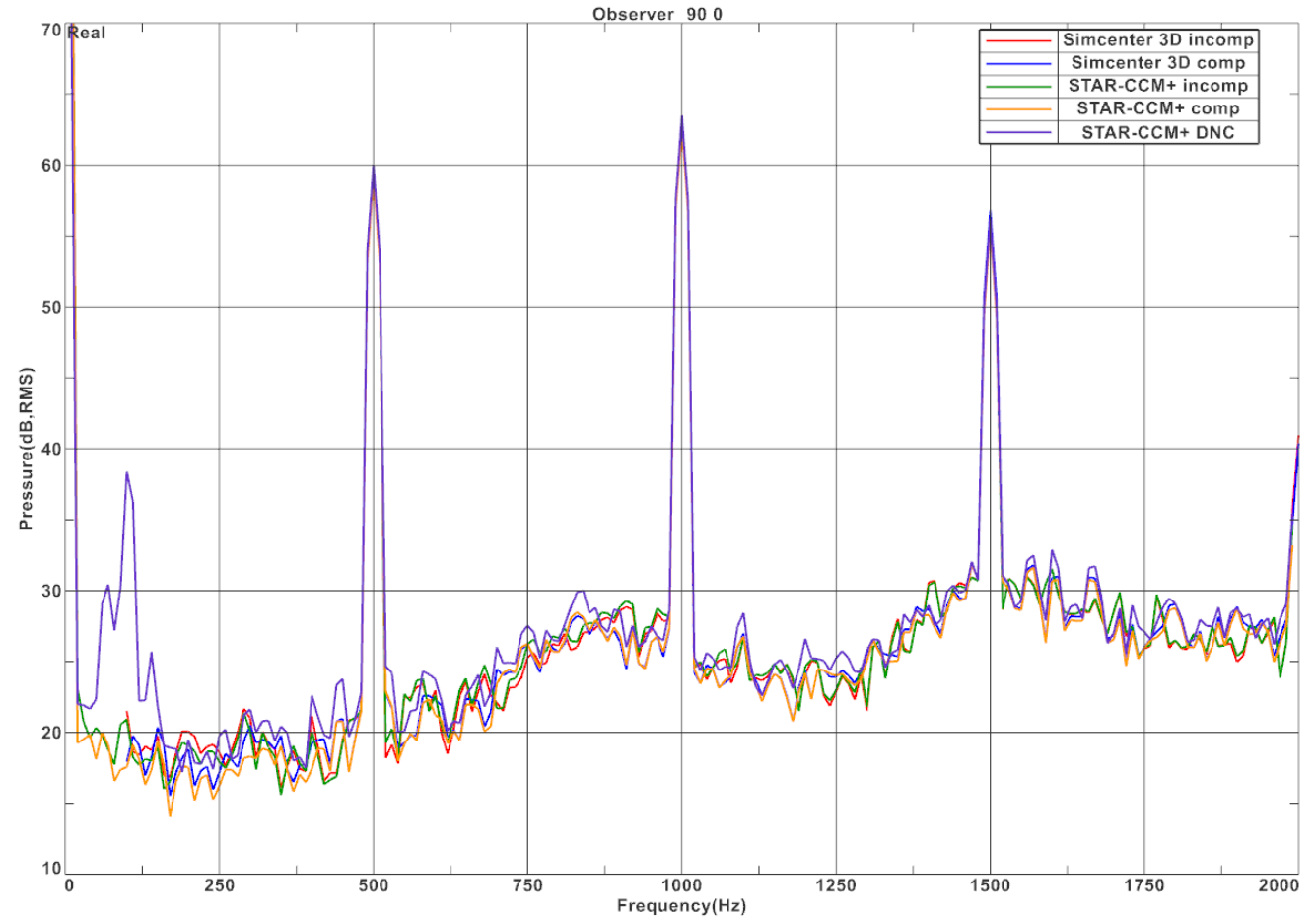
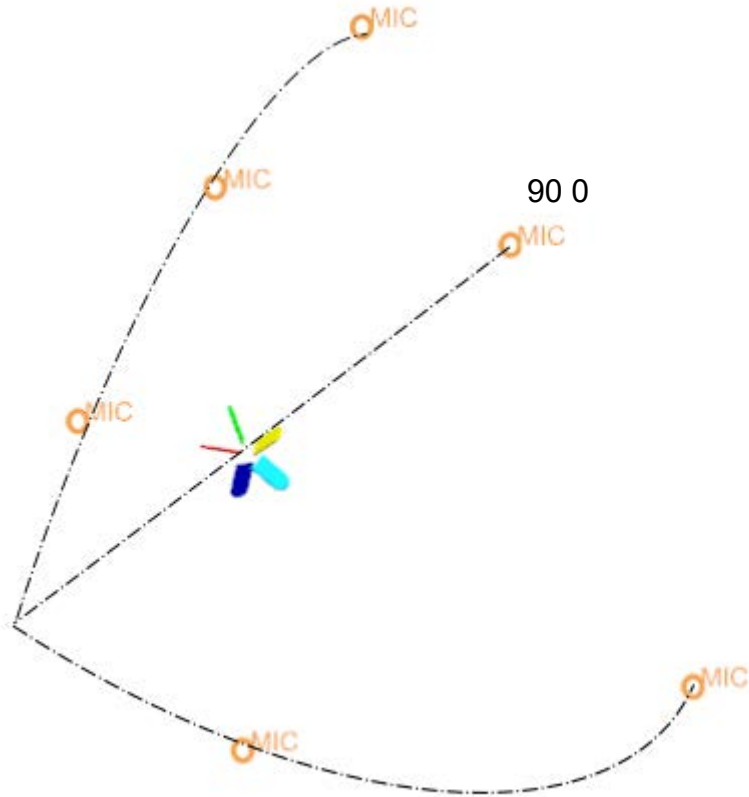
Two separate CFD inputs are considered

- **With incompressible CFD input**
to compare hybrid and FWH approaches
- **With compressible CFD input**
to compare hybrid, FWH and DNC approaches)

The goal of this comparison is to have

- same sound levels at Blade Passing Frequency (BPF) and harmonics
- similar broadband levels
- DNC solution is assumed to be the reference solution

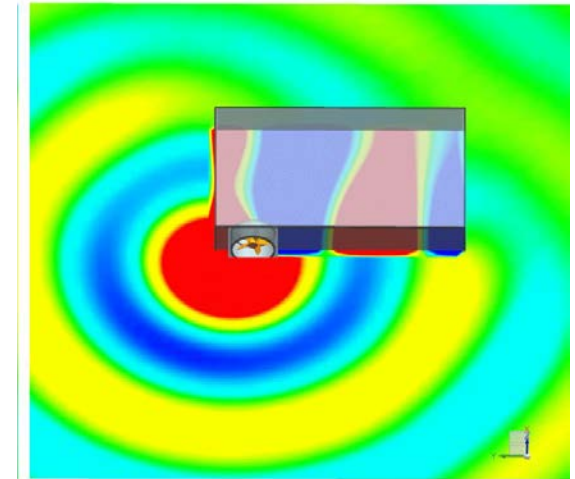
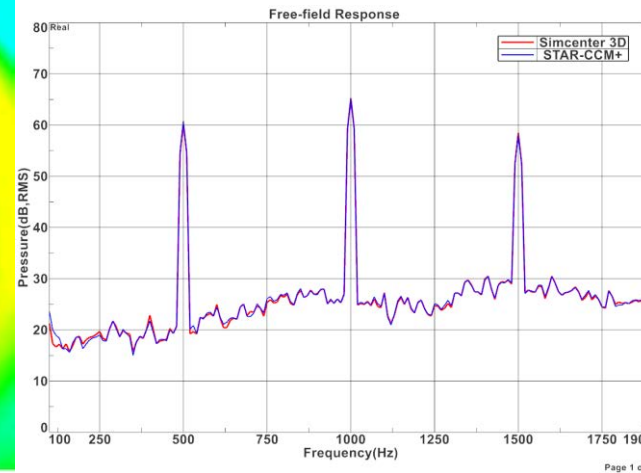
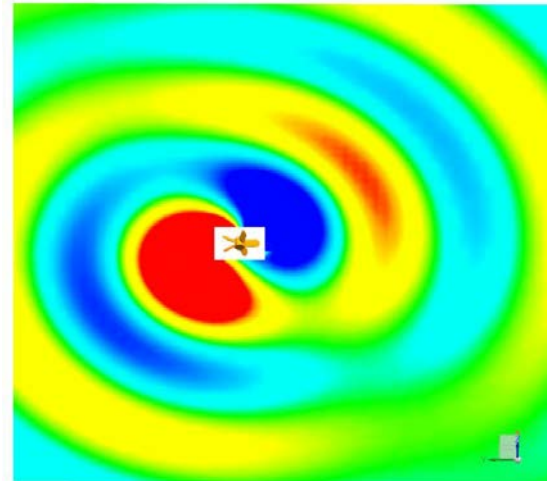
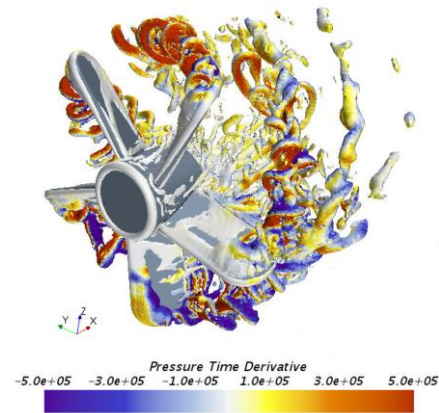
Cooling Fan Noise Simulations with Simcenter STAR-CCM+ and Simcenter 3D



All 5 methods provide similar SPL results for both tones and broadband frequencies

Cooling Fan Noise Simulations

with Simcenter STAR-CCM+ and Simcenter 3D



Compute unsteady flow field around source region with Simcenter STAR-CCM+

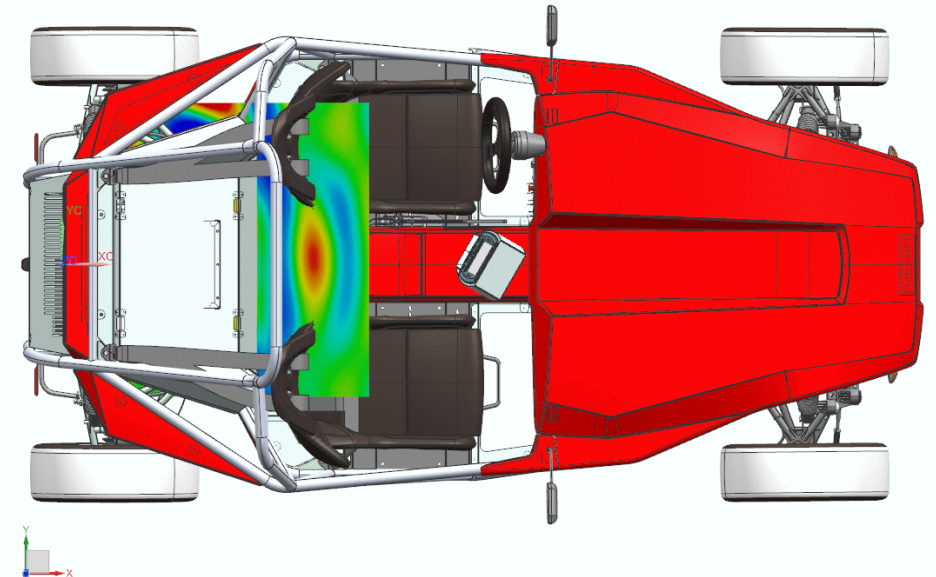
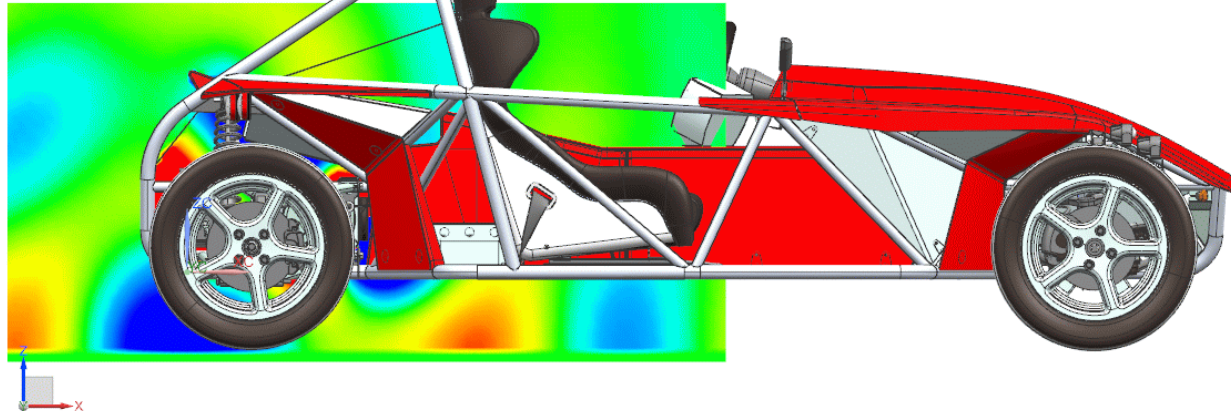
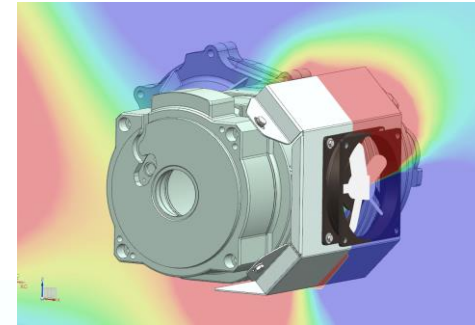
Using the transient blade pressure, compute free-field acoustic propagation with STAR-CCM+ FW-H or Simcenter 3D

Add installation effects, reflective/absorbing surface, infinite plates, porous volumes in Simcenter 3D

EM Cooling Fan Noise Simulations

with absorbing and reflective surfaces

Acoustic wave propagation from cooling fan from engine bay towards driver's ear with absorbing surfaces such as panels and seats



Aeroacoustics simulation workflow



Aerodynamic load preparation

Prepare aerodynamic loads smoothly for the aeroacoustic problem

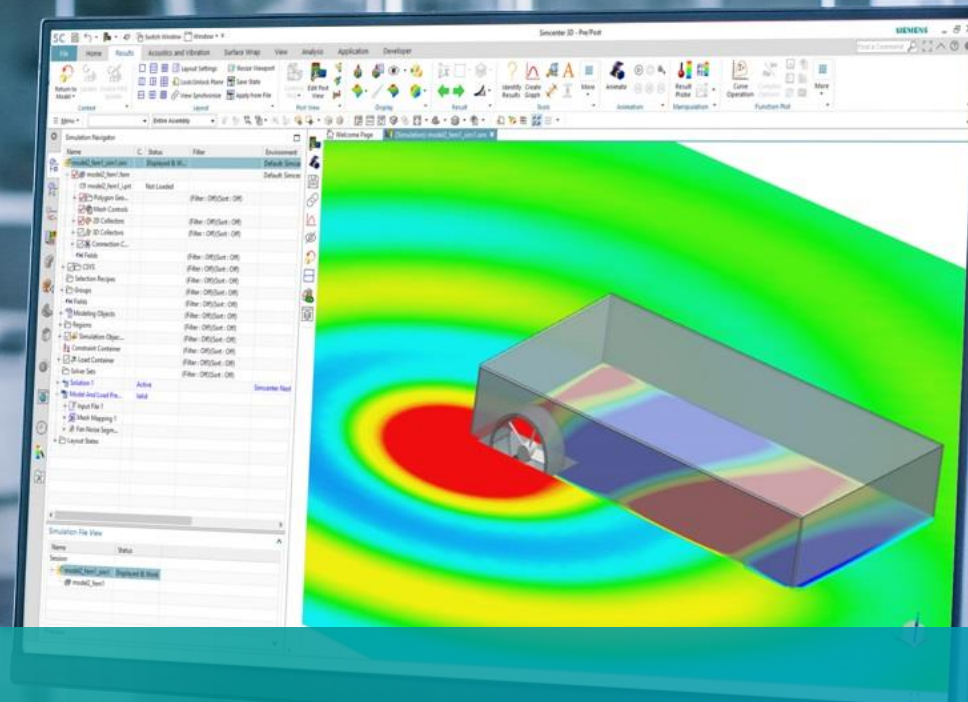
Aeroacoustic source modeling

Computation of the advanced aeroacoustics sources for rotating components

Acoustic propagation

Efficient finite element computation using single coarse physical mesh for all frequencies of interest

SIEMENS
Ingenuity for life



Questions?